## LAMPIRAN - LAMPIRAN

#include <STM32F4ADC.h>
#define D1 PE0
#define D2 PE1
#define D3 PB9
#define D4 PB8

int i=1000; int S1,S2,S3,S4,S5,S6; STM32ADC inADC(ADC1); const int setOverflow = 4000; int count,car1,car2; int refv,iact,iload,ipv,actv,err,mod\_final,car,pot,iref; double itg,lastitg,pi,mod,Bmod,P,I; uint16\_t analog\_pins[] = {PA0, PA1, PA2, PA3, PA4, PA5, PA6};

#### //control

float kp=0.2; float ki=50;

void PINMODE() {
 pinMode(D1, OUTPUT);
 pinMode(D2, OUTPUT);
 pinMode(D3, OUTPUT);
 pinMode(D4, OUTPUT);

#### }

void setup() {
 Serial.begin(9600);
 PINMODE();
 for (uint8\_t x = 0; x<sizeof(analog\_pins); x++)
 pinMode(analog\_pins[x], INPUT\_ANALOG);</pre>

Timer2.init(); Timer2.pause(); Timer2.setMasterMode(TIMER\_MASTER\_MODE\_UPDATE); Timer2.setPeriod(3000); Timer2.setMode(TIMER\_CH2, TIMER\_OUTPUT\_COMPARE); Timer2.setCompare(TIMER\_CH2, 1); Timer2.attachInterrupt(TIMER\_CH2, 1); Timer2.refresh(); Timer2.resume(); Timer3.init(); //PWM timer Timer3.setPeriod(20); Timer3.refresh(); Timer3.resume();

delayMicroseconds(19); //carrier phase delay

Timer4.init(); Timer4.setPeriod(20); Timer4.refresh(); Timer4.resume();

pinMode(PB0,PWM);
pinMode(PB6,PWM);
pinMode(PB7,PWM);
pinMode(PB8,PWM);

inADC.setSamplingTime(ADC\_SMPR\_3); inADC.enableDMA();

void loop() {
 while(1){
 sensor();
 bidirect();

}

//Serial.println(R\_acti);

void sensor(){

```
refv = map(analogRead(PA0),0,4095,-2000,2000);//referensi voltage
iact = map(analogRead(PA1),0,4095,-2000,2000);//act arus
iload = map(analogRead(PA2),0,4095,-2000,2000);//act arus
ipv = map(analogRead(PA3),0,4095,-2000,2000);//act arus
actv = map(analogRead(PA4),0,4095,-2000,2000);//actual
pot = map(analogRead(PA5),0,4095,-2000,2000);//potensio
}
```

```
void bidirect(){
```

// refv = 4000;

- iref= iload-ipv; err = iref-iact;
- P = kp\*err;
- itg = lastitg+err\*0.0001;
- I=ki\*itg;

```
mod = pi;
if(mod<-2500) //limiter
mod= -2500;
if(mod>-2500 && mod<3360)//anti windup
{
lastitg=itg;
}
```

KIX

Bmod = -mod; //*boost* mod

pwmWrite(PB6,mod); //S1 pwmWrite(PB7,Bmod); //S2 pwmWrite(PB8,Bmod); //S3 pwmWrite(PB0,mod); //S4

## } void INT1()

{

Serial.print(ipv); Serial.print(""); Serial.print(iload); Serial.print(""); Serial.println(iact);



Iranian (Iranica) Journal of Energy & Environment

Journal Homepage: wwwijeenet



IJEE an official peer review journal of Babol Noshirvani University of Technology, ISSN:2079-2115

# Control Strategy in DC Microgrid for Integrated Energy Balancer: Photovoltaic Application

#### L. H. Pratomo\*, L. A. Matthias

Department of Electrical Engineering, Faculty of Engineering, Soegijapranata Catholic University, Semarang 50234, Indonesia

PAPER INFO

A B S T R A C T

Paper history: Received 25 April 2022 Accepted in revised form 31 May 2022

Keywords: Bidirectional converter Bidirectional DC-DC Buck-boost converter Energy balancer DC micro grid Renewable energy is energy that can be used indefinitely. As a result, renewable energy sources such as solar photovoltaics developed. Conventional converters, typically used to connect the microgrid to the battery, only change the voltage. To link the microgrid to the battery, bidirectional converters are required. A bidirectional converter is available in a variety of configurations. The control structure is highly sophisticated to obtain a satisfactory output. This article proposes a bidirectional DC-DC buck-boost converter for controlling current in DC microgrids, solar systems, and loads. A bidirectional DC-DC Buck-Boost converter is required to transmit and receive energy from the battery to the DC microgrid. When voltage is sent to the DC microgrid, the battery voltage. This converter produces a better output voltage than an AC-DC Buck-Boost Converter, and its switching frequency is double that of typical converters. The modified DC-DC converter has the simplest form and the advantage of having the highest responsiveness.

doi: 10.5829/ijee.2022.13.04.02

#### INTRODUCTION

Along with the times, advanced technological improvements are implemented to create a new electrical energy source. Currently, electrical energy is the main thing needed by many people [1-3]. Therefore, many technologies have been developed to produce electrical energy from renewable energy sources, one of which comes from solar energy. The system converts solar energy into electrical energy using a PV module stored in a battery with a DC energy source [4]. A DC-AC converter is needed to convert the electricity generated by PV to AC electricity. When the conversion process occurs, there is a loss of energy from electricity. Therefore, a DC microgrid avoids energy loss in the conversion process on the DC-DC converter [5-8].

A microgrid combines loads, energy storage systems, and micro-generators. Microgrid control is an important issue to make a microgrid a single controllable unit [9-10]. The microgrid control strategy is realized by converter control. Photovoltaic sources are emission-free and reliable. The benefits of a microgrid include high constant [11]. Therefore, a PV system connected to a DC microgrid is a viable energy source. Solar PV-based DC microgrids can be cheap, flexible, and energy-efficient for users. PV has a detriment when it comes to low DC voltages. Thus, the PV cannot correctly supply the load [12]. Therefore, using a DC converter connected to a DC Microgrid produces a ripple-free output voltage and outputs current [13, 14]. The voltage generated by the PV is used to charge the battery. When the battery is in use, a converter must step up the voltage because the battery voltage is higher than the microgrid voltage and step down the voltage to send energy from the battery to the microgrid. These processes need to use a buck-boost converter. When sending and receiving power requires a converter that can do both things, a bidirectional converter is required [15-17]. The distribution system works in parallel and consists of a microgrid DC, PV, and bidirectional buck-boost converter.

The detriment of the conventional converter used on the microgrid can only lower the voltage. A bidirectional converter is needed to send and receive voltage from the battery to the grid. There are several types of bidirectional

<sup>\*</sup>Corresponding Author Email: *leonardus@unika.ac.id* (L.H. Pratomo)

Please cite this article as: L. H. Pratomo, L. A. Matthias, 2022. Control Strategy in DC Microgrid For Integrated Energy Balancer: Photovoltaic Application, Iranian (Iranica) Journal of Energy and Environment, 13(4), pp. 333-339. Doi: 10.5829/ijee.2022.13.04.02

converters. To get good output results, a complex converter structure is needed. This modified converter work at three levels [18,19]. Therefore, this paper proposes A Buck-Boost converter bidirectional DC-DC with a microgrid DC energy balancer to be used as a current balancer. The modified converter uses two diodes, four energy semiconductor switches, and two capacitors to perform 3-levels. The operating model is based upon a phase-shifted carrier signal [20-23]. The current balancing system controls the current in DC microgrids, photovoltaic systems, and loads. Current flow in the DC microgrid, photovoltaic system, and load determine whether the converter uses, sends energy to the DC grid, or receives power from the DC grid.

#### **MATERIAL AND METHODS**

#### **DC-DC microgrid configuration**

This converter operates in 2 modes, namely buck mode and boost mode. Buck mode is used to lower the voltage from the battery when sending voltage to the DC microgrid. When buck mode is used, only two energy switches are used, namely switches S1 and S4. Boost mode is used to increase the voltage from the DC microgrid, which has a lower voltage than the battery with a higher voltage. When the boost mode is used, only two energy switches are operating, namely the S2 and S3.

Figure 1 is a configuration circuit of A Buck-Boost converter bidirectional DC-DC. The PV distribution system helps absorb solar energy and produce DC voltage output. During the day, the load used tends to be lower than the load at night, and the voltage generated by PV during the day is more significant. The supply voltage on the load comes from the DC grid and the PV. Because the voltage sent from the PV to the load is small, the voltage is sent to the converter to charge the battery. When charging the battery, the converter uses the boost method to increase the voltage because the voltage from the battery is greater than the voltage on the DC grid.

At night the load used is more significant therefore, the supply voltage from the grid to meet the requirements of the load is less than the battery and supply voltage to

Figure 1. DC microgrid configuration

the load because PV does not produce voltage at night. In this method of operation, the converter use bucks mode to lower the voltage from the battery and send it to the DC grid.

There is one condition where the converter is not sending and receiving energy. This happens when the current generated by the PV is equal to the current required by the load. Then the PV supplies only to the load therefore, the converter does not receive energy, and the converter also does not send energy because the load used has received enough power from the PV. This condition is called a balanced condition, where the PV current is equal to the load current.

#### **Control strategy**

Figure 2 shows an energy circuit and control to configure the DC microgrid, DC-DC converter, and load. This control system has three ways of working: PV sends energy to the load and converter, PV sends power to the load, and PV sends energy to the converter. This system determines how the converter works when sending and receiving energy.

In the first operation, the energy generated by the PV is sent to the DC microgrid. When the load on the DC microgrid is small, the power is sent to the converter to charge the battery. The load gets energy from the DC microgrid and PV in this operation. The battery receives energy from the DC microgrid and PV. The voltage on the grid is the same. Therefore, the energy flow is the same as the current flow. The battery is charged using energy from the PV using the boost mode of the converter. This operation can be formulated as Equation (1).

$$I_{Balancer} = I_{Load} - I_{PV}$$

In the second operation, the load used is significant. The energy required on the load is also more incredible

(1)



Figure 2. System control connections

therefore, the power from the PV is sent to the load to meet the necessary energy. When the energy transmitted from the PV to the balancer is lacking, the balancer sends power to the load using the buck mode of the converter, and it can be formulated as Equation (2).

$$I_{Load} = I_{Balancer} + I_{PV} \tag{2}$$

In the third operation, the load used requires sufficient energy. PV work to send power to the DC microgrid to meet the energy requirements of the load. Still, PV cannot transmit energy to the converter because the energy required by the load is as considerable as the energy generated by PV. In this condition, the converter is not working. This operation can be formulated as Equations (3 and 4).

$$I_{Load} = I_{PV} \tag{3}$$

$$I_{Balancer} = 0 \tag{4}$$

#### **Operation modes and switching**

Based on Table 1, rows 1-4, the switching cycle of the buck operating mode, and Figure 3, where the current flow and output voltage are observable in Table 1. The output voltage measured here is the output before the inductor filter to see the switching process, and the voltage after the inductor filter is the same as the DC grid voltage. In the first operation, the energy switches used are switches S1 and S4. When switches S1 and S4 are on simultaneously, it produces the same voltage output as the battery (E). In this operating system, the current flows from the battery to switches S1 and S4 and then to the filter L, the DC grid.

The second operating system where the energy switch is used here is only the S1 switch, while the other switches are turned off. When current flows, C1 wastes energy while C2 fills power. Hence, The current flows from S1 to the battery and plugs into the capacitor C2. The current flows to the diode S3 and goes to the inductor filter (L) sent to the DC grid. When the two capacitors have a balanced voltage in this operating system, the DC grid is half the battery voltage (E/2).

The third operating system where the energy switch is used is only the S4 switch, while the other switches are turned off. The current flows from the diode on S3, fills C1 to S1, and flows into the L filter, while C2 wastes energy. When the voltage on the capacitor is balanced, the voltage on the DC grid is half of the battery voltage (E/2).

The fourth operating system where all energy switches are in the off position. The operating system that occurs is freewheeling. The voltage flow continues until the voltage slowly drops and runs out in this operation. Then the output voltage to the grid is zero volts. When operating, the current flows from diode S2 to S3 and then to the DC grid. The resulting output voltage can be formulated in Equation (5) below in the four operating modes when the converter works in buck mode.

$$V_o = V_{in} \, x \, D \tag{5}$$

In boost mode, seen in Table 1, rows 5-6, and Figure 4, where the current flows. The first operation of energy switches S2 and S3 are ON. When S2 and S3 are ON, the same as short-circuiting the converter's output, the voltage generated here is zero, and the current is stored in the filter L.

In the second operation, the energy switch S2 and S3 are OFF therefore, at this time, the current in the filter L flows to the diodes at S1 and S4 and then charges the battery. The resulting voltage at the converter's output is equal to the voltage at the battery. This operating system can be formulated with the Equation (6) below. In Equations (5 and 6),  $V_0$  is the output voltage,  $V_{in}$  is the input voltage, and in this equation, D is the duty cycle. The duty cycle is the ratio between the ON time and the period.

$$\frac{V_o}{V_{in}} = \frac{1}{1-D} \tag{6}$$





Table 1	. Switching	PWM,	output,	and mode

PWM				¥74	MODE
<b>S1</b>	S2	<b>S</b> 3	<b>S4</b>	- vout	MODE
ON	OFF	OFF	ON	Е	
ON	OFF	OFF	OFF	E/2	BUCK
OFF	OFF	OFF	ON	E/2	
OFF	OFF	OFF	OFF	0	
OFF	ON	ON	OFF	0	BOOST
OFF	OFF	OFF	OFF	Е	

L. H. Pratomo and L. A. Matthias / Iranian (Iranica) Journal of Energy and Environment 13(4): 333-339, 2022

#### **Control algorithm**

The control algorithm of the energy balancer converter is observable in Figure 4. The controller reads the output current as feedback, the current from the load, and the current from the PV. Here there is a proportional-integral (PI) controller used. First, the current reading from the load and PV is calculated, generating the first error current signal. The first error current signal is calculated with the output current from the output to produce a second error current signal that the PI controller processes. The output signal from the PI controller must be given a limiter. Therefore, the current follows the ability of the battery so as not to damage the battery. Then the output signal is processed for carrier signal modulation to produce PWM, which is used to control the energy switch of the bidirectional converter. The resulting signal from the converter pass through a filter therefore, the output signal has less noise.  $K_p$  is the proportional gain,  $K_i$  is the integrator gain, e(t) is the error value, and dt is the change of time. By using the PI controller, the steady-state error is close to zero. The program flowchart is observable in Figure 5.

#### **RESULTS AND DISCUSSION**

This bidirectional buck-boost converter was proposed and simulated using Power Simulator Software. After being simulated, the circuit simulation from Figure 2 is implemented into hardware to prove whether the simulation runs well after becoming hardware, as shown in Figure 6 shows a hardware implementation. Parameters of simulation and hardware observable in Table 2 on hardware that has been implemented to control or program the hardware using STM32F407VET6. The current sensor detects current from the load, PV, and balancer using the current sensor HX-10P. The PWM switching is generated by driver IRFP350 controlling the power switches.

Shows in Figure 7 indicate the current from the PV source is lower than the current in the load. Therefore, the converter work in buck mode. In this condition, the current probe on the oscilloscope is at x10. The current based on simulation at the load is 4.75 A, the current in the balancer is 4.25 A, and the current from the PV source is 0.5 A. The current based on hardware at the load is 1.75 A, the current in the balancer is 1.25 A, and the current







Figure 6. Hardware implementation in laboratory test

<b>Table 2.</b> Haldwale parameters in sinulation and haldwale	Table 2	2. Hardware	parameters in	simulation	and hardware
--	---------	-------------	---------------	------------	--------------

Parameter	Value
DC microgrid voltage	$48 V_{DC}$
Battery voltage	$60 V_{DC}$
Inductor filter	5 mH
Capacitor filter C1, C2	220 uF
Load resistance	30 Ohm
Switching frequency	25 kHz



Figure 4. Control algorithm for bidirectional Buck-boost converter

from the PV source is 0.5 A. This condition is observable as Equation (2) with the buck mode converter.

When the current generated by the PV source is greater than the load, the converter work here in boost mode, as seen in Figure 8. Therefore, it can be formulated as Equation (2) when the current generated by the PV source is greater than the load, the converter work in boost mode. The current based on simulation at the load is 5 A, the current in the balancer is -1 A, and the current from the PV source is 6 A. The current based on hardware at the load is 1.75 A, the current in the balancer is 3 A. This

condition is observable the same as Equation (1). In this condition, the current in the balancer is negative because the balancer receives current to charge the battery.

Figure 9 is a state where the PV and load current are the same. The converter produces zero current or does not work. Based on the simulation, the load is 5 A, the current in the balancer is 0 A, and the current from the PV source is 5 A. The current based on hardware at the load is 1.75 A, the current in the balancer is 0 A, and the current from the PV source is 1.75 A. This condition is observable in Equations (3 and 4), called the balance condition.



Figure 9. The idle current waveform on simulation (a) and hardware (b)

#### CONCLUSION

Hardware that has been made works well as it has been simulated. The microgrid requires a converter to connect to the battery, add a renewable source to use PV, and be loaded to test it. This hardware uses three current sensors to detect the current in the converter, PV, and load. Therefore, the converter adequately controls the detected current to determine how the converter works. The detection results are handled using a PI controller's closed-loop control system. This converter work in two modes, namely bucks mode and boost mode. When in buck mode, the converter sends current from the battery to the grid to help the PV meet the current needs of the load. In boost mode, the converter receives excess current from the PV when the load supplied is overloaded, which the current sensor detects. Therefore, the converter works well to increase the voltage from the microgrid to the battery and lower the voltage from the battery to the microgrid. Observable from the experimental results is that the converter hardware produces a current that has minimal noise. The proposed implementation of this Buck-Boost converter bidirectional AC-DC with current detection works as expected with a current output with a slight ripple and simple structure.

#### ACKNOWLEDGEMENT

This work was supported by the Directorate of Research and Community Service, Directorate General of Research Strengthening and Development, The Ministry of Research, Technology and Higher Education, Republic of Indonesia 2021, Grant No: 65/LL6/SP2H/TD/2021.

#### REFERENCES

- Y. Zhang, Q. Zhou, L. Zhao, Y. Ma, Q. Lv and P. Gao., 2020. Dynamic Reactive Power Configuration of High Penetration Renewable Energy Grid Based on Transient Stability Probability Assessment. 2020 IEEE 4th Conference on Energy Internet and Energy System Integration (EI2), pp. 3801-3805. Doi: 10.1109/EI250167.2020.9346594.
- Mahmoud, A., Saafan, S., Attalla, A., Elgohary, H., 2018. Enhancement of Rooftop Photovoltaic Array Characteristic Interconnected by Grid under Partial Shading Condition Using Cascaded DC/DC Converter. *Iranian (Iranica) Journal of Energy* & *Environment*, 9(1), pp. 24-30. Doi: 10.5829/ijee.2018.09.01.04
- Shiravi, A., Firoozzadeh, M., 2022. A Novel Proposed Improvement on Performance of a Photovoltaic/Water Pumping System: Energy and Environmental Analysis, *Iranian (Iranica) Journal of Energy & Environment*, 13(2), pp. 202-208. Doi: 10.5829/ijee.2022.13.02.11
- K. Wang, Y. Ma, P. Ding, R. Mu and R. Sun., 2018. Operation Control Strategy for Photovoltaic/Battery Micro-Grid. 2018 China International Conference on Electricity Distribution (CICED), pp.821-824. Doi: 10.1109/CICED.2018.8592593.
- S. N. Soheli, G. Sarowar, M. A. Hoque and M. S. Hasan, 2018. Design and Analysis of a DC -DC Buck Boost Converter to

Achieve High Efficiency and Low Voltage Gain by using Buck Boost Topology into Buck Topology. 2018 International Conference on Advancement in Electrical and Electronic Engineering (ICAEEE), pp.1-4. Doi: 10.1109/ICAEEE.2018.8643001.

- Z. Chen, K. Wang, Z. Li and T. Zheng, 2017. A review on control strategies of AC/DC microgrid. 2017 IEEE International Conference on Environment and Electrical Engineering and 2017 IEEE Industrial and Commercial Power Systems Europe (EEEIC / I&CPS Europe), pp.1-6. Doi: 10.1109/EEEIC.2017.7977807.
- Nupur and S. Nath, 2020. Inductor Current Ripples Minimization in Coupled SIDO Buck and Buck-Boost Converter by Gate Pulse Shifting. 2020 IEEE International Conference on Power Electronics, Drives and Energy Systems (PEDES), pp.1-6. Doi: 10.1109/PEDES49360.2020.9379406.
- Hajizadeh, A, 2014. Fuzzy/State-Feedback Control of a Non-Inverting Buck-Boost Converter for Fuel Cell Electric Vehicles. *Iranica Journal of Energy & Environment*, 5(1), pp.34-41. Doi: 10.5829/idosi.ijee.2014.05.01.06.
- L. Hou, X. Tang, X. Shi, H. Jiang, H. Liu and Y. Song, 2019.
   Research on Control Method of Energy Storage Interface for DC Micro-grid. *IEEE 3rd Conference on Energy Internet and Energy System Integration (EI2)*, pp.1579-1583. Doi: 10.1109/EI247390.2019.9061799.
- G. V. R. Sagar; T. Debela, 2019. Implementation of Optimal Load Balancing Strategy for Hybrid Energy Management System in DC/AC Microgrid with PV and Battery Storage. *International Journal of Engineering-Transactions A: Basics*, 32(10), pp.1437-1445, Doi: 10.5829/IJE.2019.32.10A.13
- S. Sukatjasakul and S. Po-Ngam, 2017. The micro-grid connected single-phase photovoltaic inverter with simple MPPT controller. 2017 International Electrical Engineering Congress (iEECON), pp.1-4. Doi: 10.1109/IEECON.2017.8075751.
- A. Ghosh and S. S. Saran, 2018. High gain DC-DC step-up converter with multilevel output voltage. 2018 International Symposium on Devices, Circuits and Systems (ISDCS), pp.1-6. Doi: 10.1109/ISDCS.2018.8379657.
- Z. W. Khan, H. Minxiao, C. Kai, L. Yang and A. u. Rehman, 2020. State of the Art DC-DC Converter Topologies for the Multi-Terminal DC Grid Applications: A Review, 2020 IEEE International Conference on Power Electronics, Smart Grid and Renewable Energy (PESGRE2020), pp.1-7. Doi: 10.1109/PESGRE45664.2020.9070529.
- B. Jyothi, P. Bhavana, B. T. Rao and M. S. K. Reddy, 2021. A Review on Various DC-DC Converters for Photo Voltaic Based DC Micro Grids, 2021 Emerging Trends in Industry 4.0 (ETI 4.0), pp.1-8. Doi: 10.1109/ETI4.051663.2021.9619280.
- N. Dubey and A. k. Sharma, 2019. Analysis of Bi-directional DC-DC Buck-Boost Quadratic Converter for Energy Storage Devices. 2019 International Conference on Communication and Electronics Systems (ICCES), pp.417-421. Doi: 10.1109/ICCES45898.2019.9002112.
- J. Tian, Wang, H., Wang, Y., Yan, J., Xu, R., Wang, F., Zhuo, F., 2021. Power Characteristics of A Novel DC-DC Converter with Carrier Phase-Shifted Control. 2021 IEEE 4th International Electrical and Energy Conference (CIEEC), pp.1-6. Doi: 10.1109/CIEEC50170.2021.9510921.
- H. Jahanghiri, S. Rahimi, A. Shaker and A. Ajami, 2019. A High Conversion Non-Isolated Bidirectional DC-DC converter with Low Stress for Micro-Grid Applications, 2019 10th International Power Electronics, Drive Systems and Technologies Conference (PEDSTC), pp.775-780. Doi: 10.1109/PEDSTC.2019.8697711.
- B. M. Kumar, A. Kumar, A. H. Bhat and P. Agarwal, 2017. Comparative study of dual active bridge isolated DC to DC converter with single phase shift and dual phase shift control techniques. 2017 Recent Developments in Control, Automation &

L. H. Pratomo and L. A. Matthias / Iranian (Iranica) Journal of Energy and Environment 13(4): 333-339, 2022

*Power Engineering (RDCAPE)*, pp.453-458. Doi: 10.1109/RDCAPE.2017.8358314.

- L. Hou, X. Tang, X. Shi, H. Jiang, H. Liu and Y. Song, 2019. Research on Control Method of Energy Storage Interface for DC Micro-grid. 2019 IEEE 3rd Conference on Energy Internet and Energy System Integration (EI2), pp.1579-1583. Doi: 10.1109/EI247390.2019.9061799.
- Mahalingam Prabhakar, 2014. High Gain DC-DC Converter using Active Clamp Circuit (RESEARCH NOTE). *International Journal of Engineering*, Transactions A: Basics, Vol. 27(1), pp.123-130. Doi: 10.5829/idosi.ije.2014.27.01a.15
- Gnana Prakash M, Balamurugan M, Umashankar S, 2014. A New Multilevel Inverter with Reduced Number of Switches. International Journal of Power Electronics and Drive System (IJPEDS). 5(1): 63-70. Available at:

https://pdfs.semanticscholar.org/a221/37e95f90f5e9c8b406b7fa5 e6a99fd382d16.pdf

- O. Rivera, M. Mauledoux, A. Valencia, R. Jimenez, O. Avilés, 2018. Hardware in Loop of a Generalized Predictive Controller for a Micro Grid DC System of Renewable Energy Sources. *International Journal of Engineering-Transactions B: Applications*, 31(8), pp.1215-1221. Doi: 10.5829/ije.2018.31.08b.08
- V. Monteiro, J. C. Tiago Sousa and J. L. Afonso, 2020. A Novel Topology of Modular Multilevel Bidirectional Non-Isolated dc-dc Converter. 2020 International Young Engineers Forum (YEF-ECE), pp. 61-66. Doi: 10.1109/YEF-ECE49388.2020.9171809.

#### COPYRIGHTS

©2021 The author(s) This is an open access article distributed under the terms of the Creative Commons Attribution (CC BY 40), which permits unrestricted use, distribution, and reproduction in any medium, as long as the original authors and source are cited No permission is required from the authors or the publishers



چکیدہ

#### Persian Abstract

انرژیهای تجدیدپذیر نوعی انرژی است که می توان به طور مداوم از آن استفاده کرد. در نتیجه، منابع انرژی تجدیدپذیر مانند سامانههای فتوولتائیک خورشیدی توسعه یافتند. مبدلهای معمولی که معمولا برای اتصال ریزشبکه به باتری استفاده میشوند، فقط ولتاژ را تغییر میدهند. برای اتصال ریزشبکه به باتری، مبدلهای دو طرفه مورد نیاز است. یک مبدل دوجهته در پیکربندیهای مختلف موجود است. ساختار کنترل برای به دست آوردن خروجی رضایت بخش بسیار پیچیده است. این مقاله یک مبدل تقویت کننده باک دوطرفه DC-DC برای کنترل جریان در ریزشبکههایDC ، سیستمهای خورشیدی و بارها پیشنهاد میکند. یک مبدل دوطرفه DC-DC Buck-Boost باک دوطرفه مال مختلف موجود است. ساختار کنترل برای به دست آوردن خروجی رضایت بخش بسیار میکند. یک مبدل دوطرفه DC-DC Buck-Boost باک دوطرفه کمورت انرژی از باتری به ریزشبکههایDC ، سیستمهای خورشیدی و بارها پیشنهاد میکند. یک مبدل دوطرفه مورد نیاز است. های دوطرفه DC-DC برای انتقال و دریافت انرژی از باتری به ریزشبکههایDC موردنیاز است. هنگامی که ولتاژ بر ریزشبکه میکند. یک مبدل دوطرفه Ac-DC Buck-Boost برای انتقال و دریافت انرژی از باتری به ریزشبکه مایت موردنیاز است. هنگامی که ولتاژ بر دوجی میکند. یک مبدل دوطرفه می میداید. در غیر این صورت، هنگامی که باتری با ولتاژ شارژ میشود، ولتاژ شارژ افزایش می باید. این مبدل ولتاژ خروجی بهتری نسبت به مبدل AC-DC Buck-Boost ایرتی با می می ولتاژ شارژ می مولی است. مبدل DC-DC اصلاح شده دارای ساده ترین شکل و مزیت آن، داشتن بالاترین پاسخگویی است.

POIJAPRAT

#### PAPER NAME

18.F1.000\_Lauw Albert Matthias

### AUTHOR

Lauw Albert Matthias

WORD COUNT

4631 Words

PAGE COUNT

36 Pages

SUBMISSION DATE

May 30, 2022 7:37 AM GMT+7

CHARACTER COUNT

28506 Characters

FILE SIZE

4.2MB

REPORT DATE

May 30, 2022 7:38 AM GMT+7

## • 6% Overall Similarity

The combined total of all matches, including overlapping sources, for each database.

GIJA

- 5% Internet database
- Crossref database
- 4% Submitted Works database

## Excluded from Similarity Report

- Bibliographic material
- Cited material

- 2% Publications database
- Crossref Posted Content database
- Quoted material
- Small Matches (Less then 10 words)