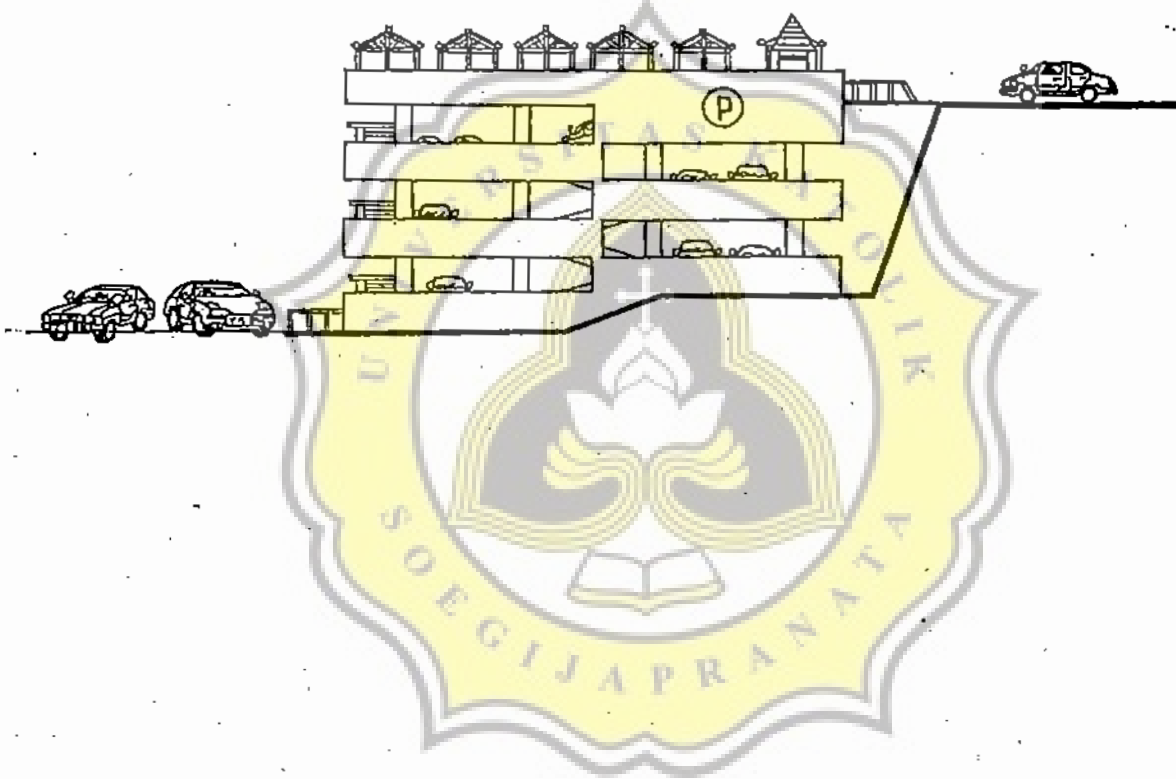
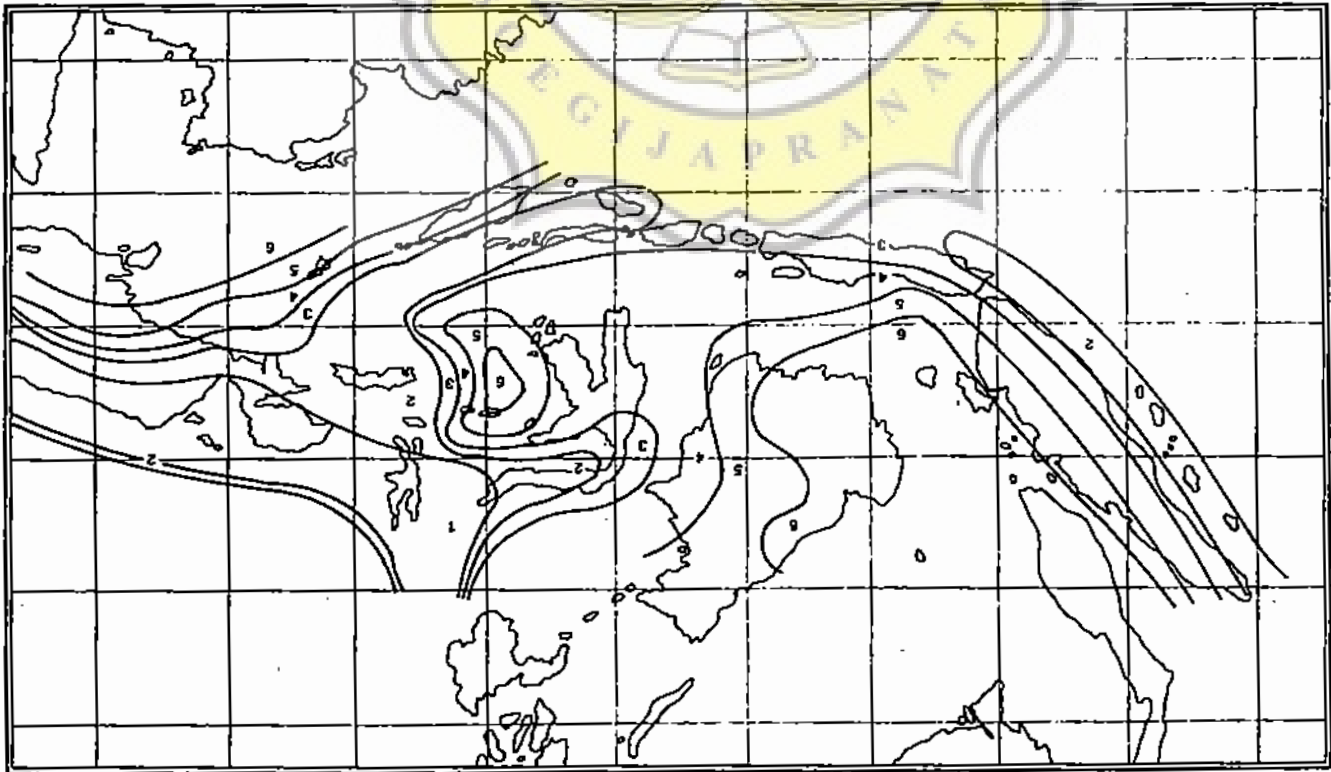


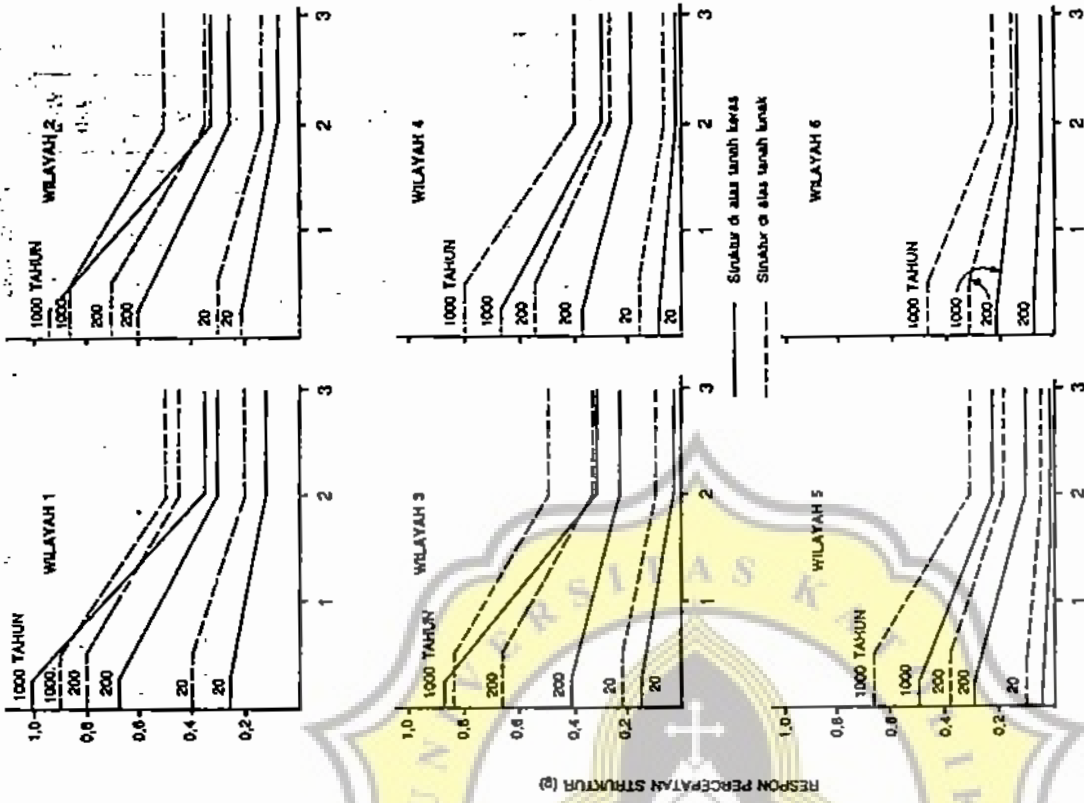
## LAMPIRAN



PERENCANAAN GEDUNG PARKIR  
UNIVERSITAS KATOLIK SOEGIJAPRANATA  
SEMARANG



Gambar 2-4 Peta wilayah gempa di Indonesia [12].



Gambar 2-5 Respon percepatan struktur [12].



5.1.d MUTU BETON  $f'_c$  30

$\phi = 0,8$

$M_u$ / kNm <sup>2</sup>	$f'_c = 240$ MPa		$f'_c = 400$ MPa		c/d	z/d
	$\rho$	$a_n$	$\rho$	$a_n$		
100	0,0005	0,192	0,0003	0,319	0,006	0,998
200	0,0010	0,191	0,0006	0,318	0,012	0,995
300	0,0016	0,191	0,0009	0,318	0,017	0,993
400	0,0021	0,190	0,0013	0,317	0,023	0,990
500	0,0026	0,190	0,0016	0,316	0,029	0,988
600	0,0032	0,189	0,0019	0,315	0,035	0,985
700	0,0037	0,189	0,0022	0,314	0,041	0,983
800	0,0043	0,188	0,0026	0,314	0,047	0,980
900	0,0048	0,188	0,0029	0,313	0,053	0,977
1000	0,0053	0,187	0,0032	0,312	0,059	0,975
1100	0,0059	0,187	0,0035	0,311	0,065	0,972
1200	0,0064	0,186	0,0039	0,310	0,071	0,970
1300	0,0070	0,186	0,0042	0,309	0,078	0,967
1400	0,0076	0,185	0,0045	0,309	0,084	0,964
1500	0,0081	0,185	0,0049	0,308	0,090	0,962
1600	0,0087	0,184	0,0052	0,307	0,096	0,959
1700	0,0093	0,184	0,0056	0,306	0,103	0,956
1800	0,0098	0,183	0,0059	0,305	0,109	0,954
1900	0,0104	0,183	0,0062	0,304	0,115	0,951
2000	0,0110	0,182	0,0066	0,303	0,122	0,948
2200	0,0122	0,181	0,0073	0,302	0,135	0,943
2400	0,0133	0,180	0,0080	0,300	0,148	0,937
2600	0,0145	0,179	0,0087	0,298	0,161	0,932
2800	0,0158	0,178	0,0095	0,296	0,174	0,926
3000	0,0170	0,177	0,0102	0,294	0,188	0,920
3200	0,0182	0,176	0,0109	0,293	0,202	0,914
3400	0,0195	0,174	0,0117	0,291	0,216	0,908
3600	0,0208	0,173	0,0125	0,289	0,230	0,902
3800	0,0221	0,172	0,0133	0,287	0,245	0,896
4000	0,0234	0,171	0,0140	0,285	0,259	0,890
4200	0,0248	0,170	0,0149	0,283	0,274	0,883
4400	0,0261	0,168	0,0157	0,281	0,289	0,877
4600	0,0275	0,167	0,0165	0,279	0,305	0,870
4800	0,0289	0,166	0,0174	0,276	0,320	0,864
5000	0,0304	0,165	0,0182	0,274	0,336	0,857
5200	0,0319	0,163	0,0191	0,272	0,253	0,850
5400	0,0334	0,162	0,0200	0,270	0,369	0,843
5600	0,0349	0,160	0,0209	0,267	0,386	0,836
5800	0,0365	0,159	0,0219	0,265	0,404	0,828
6000	0,0381	0,158	0,0228	0,263	0,422	0,821
6200	0,0397	0,156	0,0238	0,260	0,440	0,813
6400	0,0414	0,155	0,0248	0,258	0,458	0,805
6600	0,0431	0,153			0,478	0,797
6800	0,0449	0,151			0,497	0,789
7000	0,0467	0,150			0,518	0,780
7200	0,0486	0,148			0,538	0,771

5.1.i MUTU BETON  $f'_c$  30 $\phi = 1$ 

M/d <sup>2</sup>	$f = 240 \text{ MPa}$		$f = 400 \text{ MPa}$		c/d	z/d
	$\rho$	$\mu_u$	$\rho$	$\mu_u$		
100	0,0004	0,240	0,0003	0,399	0,005	0,998
200	0,0008	0,239	0,0005	0,398	0,009	0,996
300	0,0013	0,239	0,0008	0,398	0,014	0,994
400	0,0017	0,238	0,0010	0,397	0,019	0,992
500	0,0021	0,238	0,0013	0,396	0,023	0,990
600	0,0025	0,237	0,0015	0,395	0,028	0,988
700	0,0030	0,237	0,0018	0,394	0,033	0,986
800	0,0034	0,236	0,0020	0,394	0,038	0,984
900	0,0038	0,236	0,0023	0,393	0,042	0,982
1000	0,0043	0,235	0,0026	0,392	0,047	0,980
1100	0,0047	0,235	0,0028	0,391	0,052	0,978
1200	0,0051	0,234	0,0031	0,390	0,057	0,976
1300	0,0056	0,234	0,0033	0,390	0,062	0,974
1400	0,0060	0,233	0,0036	0,389	0,066	0,972
1500	0,0064	0,233	0,0039	0,388	0,071	0,970
1600	0,0069	0,232	0,0041	0,387	0,076	0,968
1700	0,0073	0,232	0,0044	0,386	0,081	0,965
1800	0,0078	0,231	0,0047	0,385	0,086	0,963
1900	0,0082	0,231	0,0049	0,384	0,091	0,961
2000	0,0087	0,230	0,0052	0,384	0,096	0,959
2200	0,0096	0,229	0,0058	0,382	0,106	0,955
2400	0,0105	0,228	0,0063	0,380	0,116	0,950
2600	0,0115	0,227	0,0069	0,378	0,127	0,946
2800	0,0124	0,226	0,0074	0,377	0,137	0,942
3000	0,0133	0,225	0,0080	0,375	0,148	0,937
3200	0,0143	0,224	0,0086	0,373	0,158	0,933
3400	0,0153	0,223	0,0092	0,371	0,169	0,928
3600	0,0162	0,222	0,0097	0,369	0,180	0,924
3800	0,0172	0,221	0,0103	0,368	0,191	0,919
4000	0,0182	0,219	0,0109	0,366	0,202	0,914
4200	0,0192	0,218	0,0115	0,364	0,213	0,909
4400	0,0203	0,217	0,0122	0,362	0,224	0,905
4600	0,0213	0,216	0,0128	0,360	0,236	0,900
4800	0,0224	0,215	0,0134	0,358	0,247	0,895
5000	0,0234	0,214	0,0140	0,356	0,259	0,890
5200	0,0245	0,212	0,0147	0,354	0,271	0,885
5400	0,0256	0,211	0,0153	0,352	0,283	0,880
5600	0,0267	0,210	0,0160	0,350	0,295	0,874
5800	0,0278	0,209	0,0167	0,348	0,308	0,869
6000	0,0289	0,207	0,0174	0,346	0,320	0,864
6200	0,0301	0,206	0,0181	0,343	0,333	0,858
6400	0,0313	0,205	0,0188	0,341	0,346	0,853
6600	0,0325	0,203	0,0195	0,339	0,359	0,847
6800	0,0337	0,202	0,0202	0,337	0,372	0,842
7000	0,0349	0,201	0,0209	0,334	0,386	0,836
7200	0,0361	0,199	0,0217	0,332	0,400	0,830
7400	0,0374	0,198	0,0225	0,330	0,414	0,824
7600	0,0387	0,196	0,0232	0,327	0,429	0,818
7800	0,0400	0,195	0,0240	0,325	0,443	0,812
8000	0,0414	0,193	0,0248	0,322	0,458	0,805
8200	0,0428	0,192			0,474	0,799
8400	0,0442	0,190			0,489	0,792
8600	0,0456	0,188			0,505	0,785
8800	0,0471	0,187			0,522	0,778
9000	0,0486	0,185			0,538	0,771

5.3.d MUTU BETON  $f'_c$  30 dengan tulangan tekan $\phi = 0,8$ Diketahui  $\rho$  tulangan tarik,  $\rho$  tulangan tekan = 0,5  $\cdot$   $\rho$  tulangan tarik

$M_u/bd^2$	$f'_c = 240 \text{ MPa}$ $d'/d =$			$f'_c = 400 \text{ MPa}$ $d'/d =$		
	0,10	0,15	0,20	0,10	0,15	0,20
	200	0,0011	0,0011	0,0012	0,0007	0,0007
400	0,0022	0,0023	0,0023	0,0013	0,0014	0,0014
600	0,0033	0,0034	0,0035	0,0020	0,0020	0,0021
800	0,0044	0,0045	0,0047	0,0026	0,0027	0,0028
1000	0,0055	0,0057	0,0058	0,0033	0,0034	0,0035
1200	0,0066	0,0068	0,0070	0,0040	0,0041	0,0042
1400	0,0078	0,0080	0,0082	0,0046	0,0048	0,0049
1600	0,0089	0,0091	0,0094	0,0053	0,0055	0,0056
1800	0,0100	0,0103	0,0106	0,0060	0,0062	0,0063
2000	0,0111	0,0114	0,0118	0,0067	0,0069	0,0071
2200	0,0122	0,0126	0,0130	0,0073	0,0076	0,0078
2400	0,0134	0,0138	0,0142	0,0080	0,0083	0,0085
2600	0,0145	0,0149	0,0154	0,0087	0,0090	0,0092
2800	0,0157	0,0161	0,0166	0,0094	0,0097	0,0099
3000	0,0168	0,0173	0,0178	0,0101	0,0104	0,0107
3200	0,0179	0,0185	0,0190	0,0108	0,0111	0,0114
3400	0,0191	0,0196	0,0202	0,0115	0,0118	0,0121
3600	0,0202	0,0208	0,0214	0,0121	0,0125	0,0129
3800	0,0214	0,0220	0,0227	0,0128	0,0132	0,0136
4000	0,0226	0,0232	0,0239	0,0135	0,0139	0,0143
4200	0,0237	0,0244	0,0251	0,0142	0,0146	0,0151
4400	0,0249	0,0256	0,0264	0,0149	0,0154	0,0158
4600	0,0261	0,0268	0,0276	0,0156	0,0161	0,0166
4800	0,0272	0,0280	0,0289	0,0163	0,0168	0,0173
5000	0,0284	0,0292	0,0301	0,0170	0,0175	0,0181
5200	0,0296	0,0305	0,0314	0,0178	0,0183	0,0188
5400	0,0308	0,0317	0,0326	0,0185	0,0190	0,0196
5600	0,0320	0,0329	0,0339	0,0192	0,0197	0,0203
5800	0,0332	0,0341	0,0352	0,0199	0,0205	0,0211
6000	0,0344	0,0354	0,0365	0,0206	0,0212	0,0219
6200	0,0356	0,0366	0,0377	0,0213	0,0220	0,0226
6400	0,0368	0,0379	0,0390	0,0221	0,0227	0,0234
6600	0,0380	0,0391	0,0403	0,0228	0,0235	0,0242
6800	0,0392	0,0404	0,0416	0,0235	0,0242	0,0250
7000	0,0404	0,0416	0,0429	0,0242	0,0250	0,0258
7200	0,0416	0,0429	0,0442	0,0250	0,0257	0,0265
7400	0,0428	0,0441	0,0455	0,0257	0,0265	0,0273
7600	0,0441	0,0454	0,0469	0,0264	0,0272	0,0281
7800	0,0453	0,0467	0,0482	0,0272	0,0280	0,0289
8000	0,0465	0,0480	0,0495	0,0279	0,0288	0,0297
8200	0,0478	0,0493	0,0508	0,0287	0,0296	0,0305

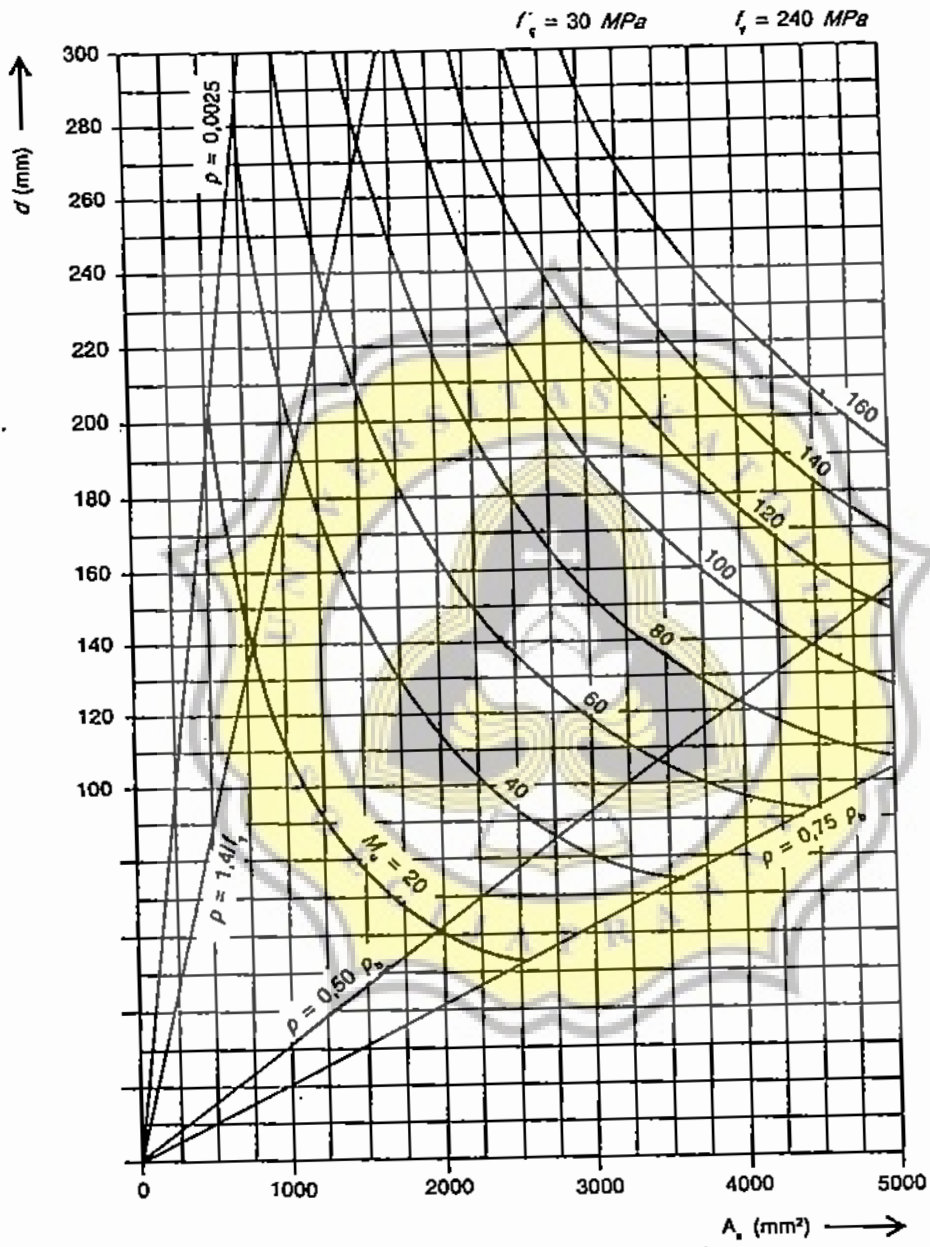


5.3.i MUTU BETON  $f'_c$  30 dengan tulangan tekan

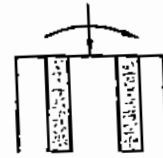
$\phi = 1$

Diketahui  $\rho$  tulangan tarik,  $\rho$  tulangan tekan = 0,5  $\cdot$   $\rho$  tulangan tarik

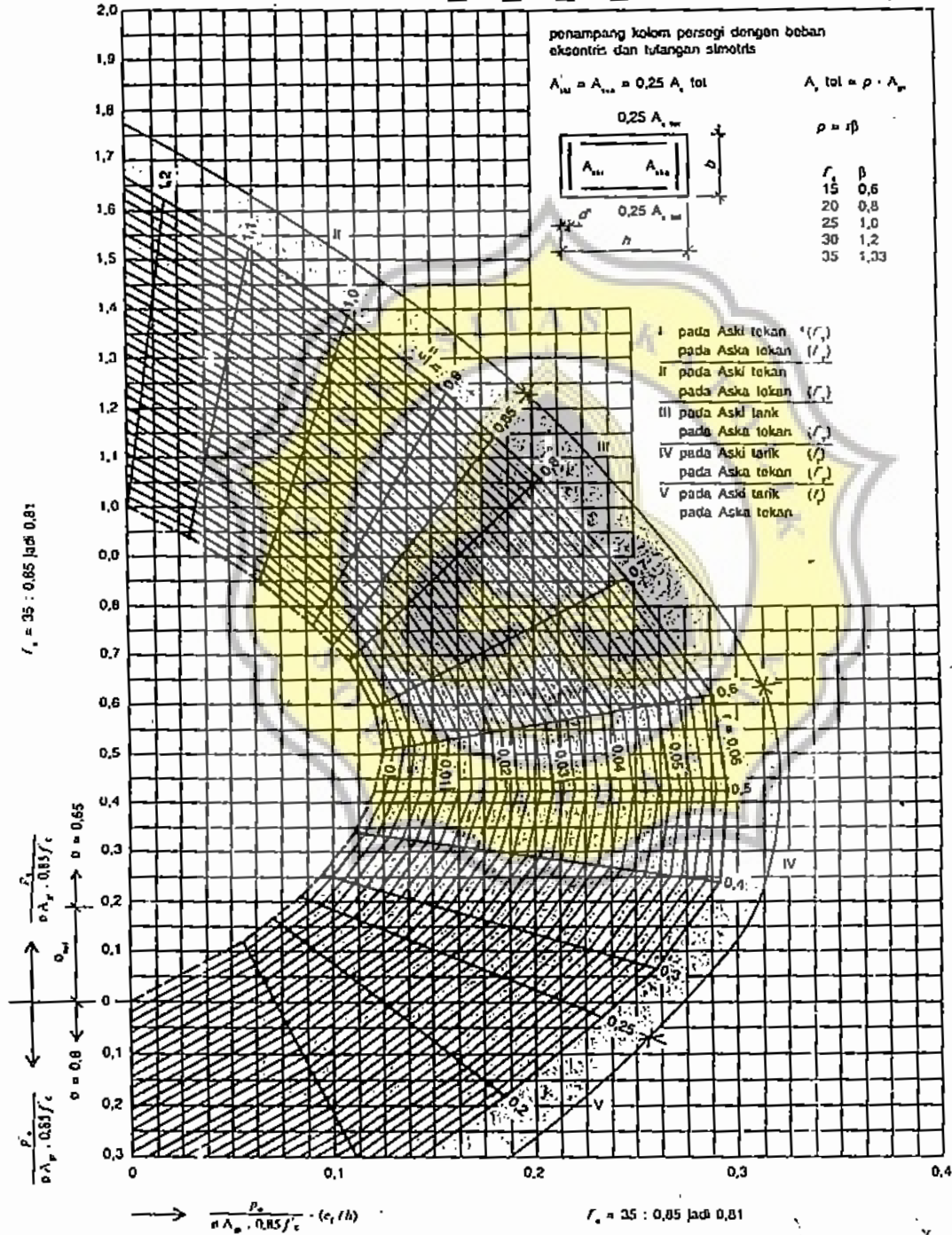
$M_u$ /bd <sup>2</sup>	$f_y = 240$ MPa $d'/d =$			$f_y = 400$ MPa $d'/d =$		
	0,10	0,15	0,20	0,10	0,15	0,20
200	0,0009	0,0009	0,0009	0,0005	0,0005	0,0006
400	0,0018	0,0018	0,0019	0,0011	0,0011	0,0011
600	0,0026	0,0027	0,0028	0,0016	0,0016	0,0017
800	0,0035	0,0036	0,0037	0,0021	0,0022	0,0022
1000	0,0044	0,0045	0,0047	0,0026	0,0027	0,0028
1200	0,0053	0,0054	0,0056	0,0032	0,0033	0,0034
1400	0,0062	0,0064	0,0065	0,0037	0,0038	0,0039
1600	0,0071	0,0073	0,0075	0,0042	0,0044	0,0045
1800	0,0080	0,0082	0,0084	0,0048	0,0049	0,0051
2000	0,0089	0,0091	0,0094	0,0053	0,0055	0,0056
2200	0,0098	0,0100	0,0103	0,0059	0,0060	0,0062
2400	0,0107	0,0110	0,0113	0,0064	0,0066	0,0068
2600	0,0116	0,0119	0,0122	0,0069	0,0071	0,0073
2800	0,0125	0,0128	0,0132	0,0075	0,0077	0,0079
3000	0,0134	0,0138	0,0142	0,0080	0,0083	0,0085
3200	0,0143	0,0147	0,0151	0,0086	0,0088	0,0091
3400	0,0152	0,0156	0,0161	0,0091	0,0094	0,0096
3600	0,0161	0,0166	0,0170	0,0097	0,0099	0,0102
3800	0,0170	0,0175	0,0180	0,0102	0,0105	0,0108
4000	0,0179	0,0185	0,0190	0,0108	0,0111	0,0114
4200	0,0189	0,0194	0,0200	0,0113	0,0116	0,0120
4400	0,0198	0,0203	0,0209	0,0119	0,0122	0,0126
4600	0,0207	0,0213	0,0219	0,0124	0,0128	0,0132
4800	0,0216	0,0223	0,0229	0,0130	0,0134	0,0137
5000	0,0226	0,0232	0,0239	0,0135	0,0139	0,0143
5200	0,0235	0,0242	0,0249	0,0141	0,0145	0,0149
5400	0,0244	0,0251	0,0259	0,0147	0,0151	0,0155
5600	0,0254	0,0261	0,0269	0,0152	0,0157	0,0161
5800	0,0263	0,0271	0,0279	0,0158	0,0162	0,0167
6000	0,0272	0,0280	0,0289	0,0163	0,0168	0,0173
6200	0,0282	0,0290	0,0299	0,0169	0,0174	0,0179
6400	0,0291	0,0300	0,0309	0,0175	0,0180	0,0185
6600	0,0301	0,0309	0,0319	0,0180	0,0186	0,0191
6800	0,0310	0,0319	0,0329	0,0186	0,0192	0,0197
7000	0,0320	0,0329	0,0339	0,0192	0,0197	0,0203
7200	0,0329	0,0339	0,0349	0,0198	0,0203	0,0210
7400	0,0339	0,0349	0,0359	0,0203	0,0209	0,0216
7600	0,0348	0,0359	0,0370	0,0209	0,0215	0,0222
7800	0,0358	0,0369	0,0380	0,0215	0,0221	0,0228
8000	0,0368	0,0379	0,0390	0,0221	0,0227	0,0234
8200	0,0377	0,0389	0,0401	0,0226	0,0233	0,0240
8400	0,0387	0,0399	0,0411	0,0232	0,0239	0,0247
8600	0,0397	0,0409	0,0421	0,0238	0,0245	0,0253
8800	0,0406	0,0419	0,0432	0,0244	0,0251	0,0259
9000	0,0416	0,0429	0,0442	0,0250	0,0257	0,0265
9200	0,0426	0,0439	0,0453	0,0256	0,0263	0,0272
9400	0,0436	0,0449	0,0463	0,0261	0,0269	0,0278
9600	0,0446	0,0459	0,0474	0,0267	0,0276	0,0284
9800	0,0456	0,0469	0,0484	0,0273	0,0282	0,0291
10000	0,0465	0,0480	0,0495	0,0279	0,0288	0,0297
10200	0,0475	0,0490	0,0506	0,0285	0,0294	0,0303
10400	0,0485	0,0500	0,0516	0,0291	0,0300	0,0310



Gambar 5.4.d



15 20 25 30 35 / 240  $d'/h = 0,15$



Gambar 6.1.e





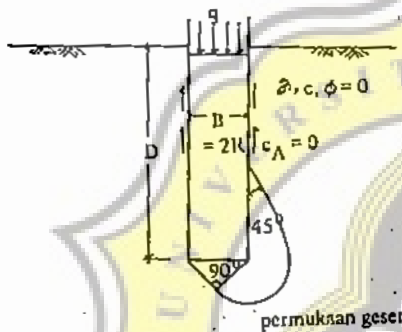
**Pondasi Dalam (Langsung) :**

Pondasi dalam kita gunakan, bila lapisan tanah di dasar pondasi yang mampu mendukung beban yang dilimpahkan, terletak cukup dalam, atau dengan pertimbangan adanya penggerusan, galian dekat pondasi dikemudian hari.

\*Daya dukung ijin tanah, (tanah cohesive & seragam).

Kondisi yang dipenuhi :

1. Tanah seragam, minimum sampai kedalaman D dibawah dasar pondasi.
2. Dasar pondasi adalah kasar.
3. Adhesi antara sisi vertikal pondasi dan tanah diabaikan.
4. Beban vertikal sentris.



Pondasi menerus :

$$q_{ult} = c \cdot N_{cc} + \gamma \cdot D$$

Pondasi bujur sangkar :

$$q_{ult} = c \cdot N_{cs} + \gamma \cdot D$$

Pondasi bulat :  $R = B/2$

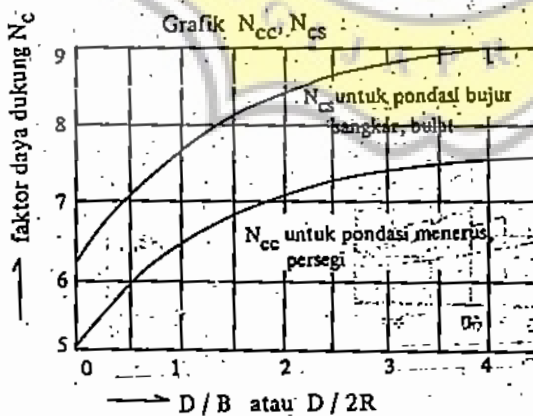
$$q_{ult} = c \cdot N_{cs} + \gamma \cdot D$$

Pondasi persegi :

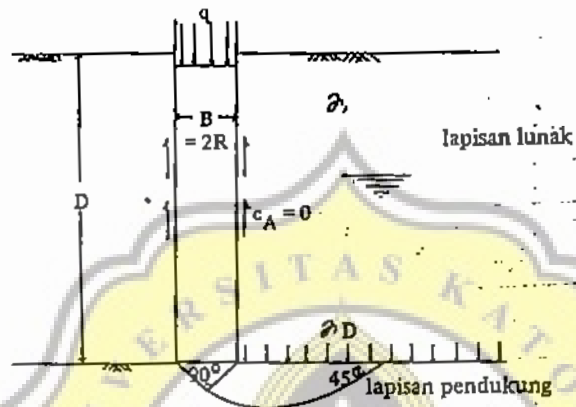
$$q_{ult} = c \cdot N_{cr} + \gamma \cdot D$$

$$N_{cr} = N_{cc} [1 + 0,2(B/L)]$$

Grafik  $N_{cc}, N_{cs}$



- \* Daya dukung ijin tanah,  
(tanah cohesive & tanah di-sisi vertikal adalah lapisan lunak)



Kondisi yang dipenuhi :

Seperti pada tanah cohesive & seragam, hanya disini kekuatan dari lapisan lunak diabaikan.

- Pondasi menerus :  
 $q_{ult} = c \cdot N_c + \phi \cdot D.$
- Pondasi bujur sangkar, bulat :  
 $q_{ult} = 1,3 \cdot c \cdot N_c + \phi \cdot D.$
- Pondasi persegi :  
 $q_{ult} = c \cdot N_c [ 1 + 0,3 (B/L) ] + \phi \cdot D.$

Nilai faktor  $N_c$ , lihat grafik  $N_c, N_q, N_\phi$ .

LAPORAN PENELITIAN TANAH

DI LOKASI GEDUNG UNIT B & C

*HENRICUS CONSTANT*

UNIKA SOEGIJAPRANATA

SEMARANG



LABORATORIUM MEKANIKA TANAH  
UNIVERSITAS KATOLIK SOEGIJAPRANATA

JL. Pawiyatan Luhur IV / 1 Bendan Duwur, Semarang - 50234

JANUARI - 1997



**LABORATORIUM MEKANIKA TANAH  
UNIVERSITAS KATOLIK SOEGIJAPRANATA**

Jl. Pawiyatan Luhur IV / 1 Bendan Dhuwur Semarang - 50234

Telp. (024) 316142 - 441555 (Hunting)

Fax. (024) 415429 E-Mail : unika@semarang.wasantara.net.id. Po. Box. 8033/SM

Badan Hukum : Yayasan Sandjojo

**PROYEK GEDUNG HENRICUS CONSTANT  
UNIKA SOEGIJAPRANATA - SEMARANG**

**Lingkup Penelitian**

- Sondir kapasitas 2.5 ton sebanyak 7 titik ( gambar terlampir )
- Bor dalam sebanyak 2 titik bor

**Rekomendasi**

***Daya Dukung Pondasi Sumuran***

Dipakai Rumus Empiris dari Reese and O Neil :

$$\begin{aligned}q_c &= 0,6 \gamma_f N_{60} < 4500 \text{ kpa} \\ &= 0,6 \cdot 100 \cdot 60 \\ &= 3600 \text{ kpa}\end{aligned}$$

Bila  $\emptyset$  sumuran  $> 50$  in di reduksi dengan persamaan

$$\begin{aligned}q_{er}' &= 4,17 \cdot \frac{B_r}{B_b} \cdot q_c \\ &= 4,17 \cdot \frac{0,3}{3} \cdot \\ &= 0,417 \cdot 3600 \\ &= 1500 \text{ kpa}\end{aligned}$$

Dengan  $sf = 2 \rightarrow q_{er}' = 750 \text{ kpa}$

Daya dukung tanah untuk pondasi sumuran dapat dipakai tidak lebih dari 7,5 kg/cm<sup>2</sup>, untuk lapisan tanah dengan SPT  $> 60$  pukulan.



LABORATORIUM MEKANIKA TANAH

UNIVERSITAS KATOLIK SOEGIJAPRANATA

Jl. Pawiyatan Luhur IV / 1 Bendan Dhuwur Semarang - 50234

Telp. (024) 316142 - 441555 (Hunting)

Fax. (024) 415429 E-Mail : unika@semarang.wasantara.net.id. Po. Box. 8033/SM

Badan Hukum : Yayasan Sandjojo

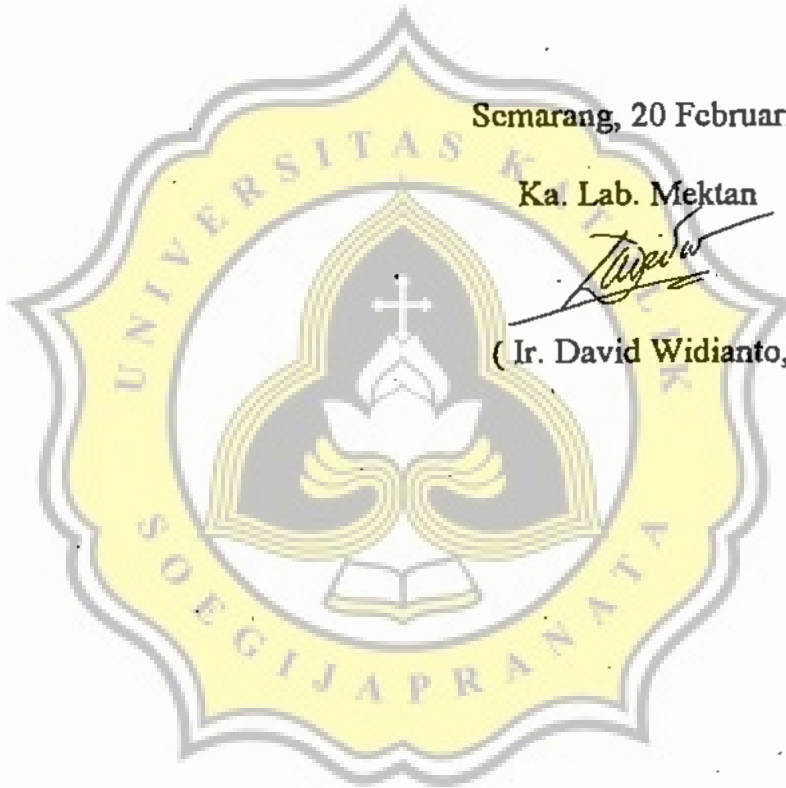
### Penutup

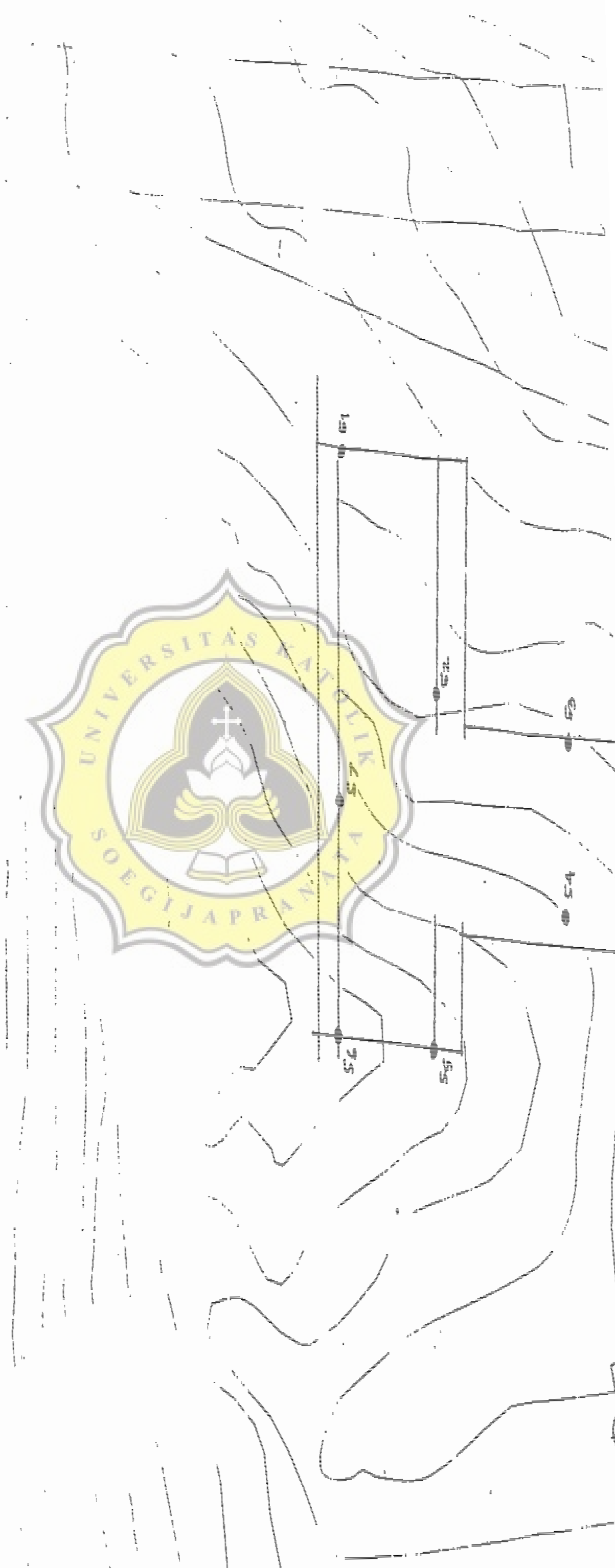
Demikian laporan kami buat atas kepercayaan yang diberikan, kami ucapkan terima kasih .

Semarang, 20 Februari 1997

Ka. Lab. Mektan

(Ir. David Widiyanto, MT)







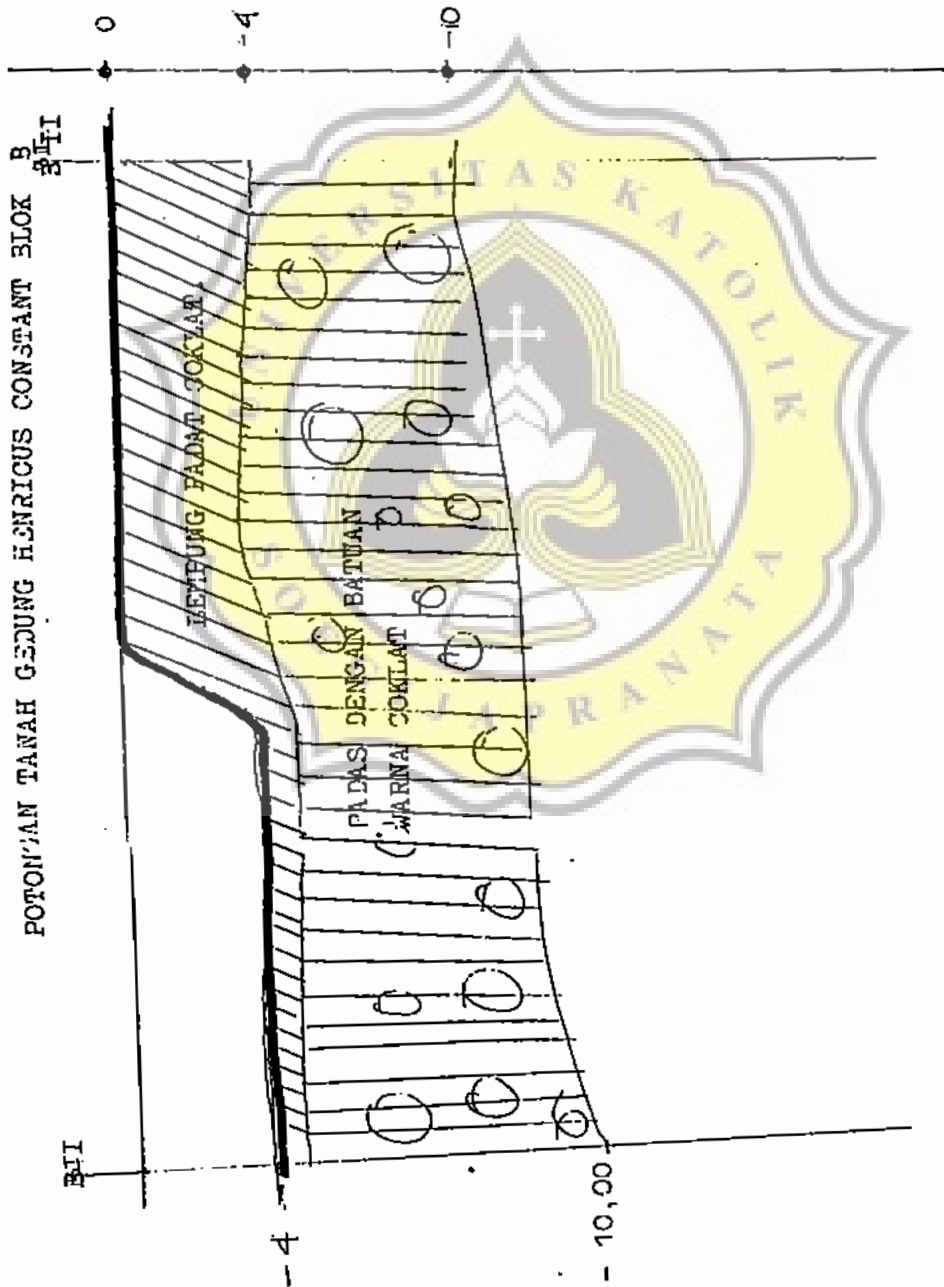
**LABORATORIUM MEKANIKA TANAH**  
**UNIVERSITAS KATOLIK SOEGIJAPRANATA**

Jl. Pawiyatan Luhur IV/1 Bendan Duwur Semarang - 50234

Telp. (024) 316142 - 441555 (hunting)

Fax. (024) 415429 E-Mail : soepra14@rad.net.id Po. Box. 8033/SM

Badan Hukum : Yayasan Sandjojo



**LAB MEKTAN UNIKA SOEGIJAPRANATA**

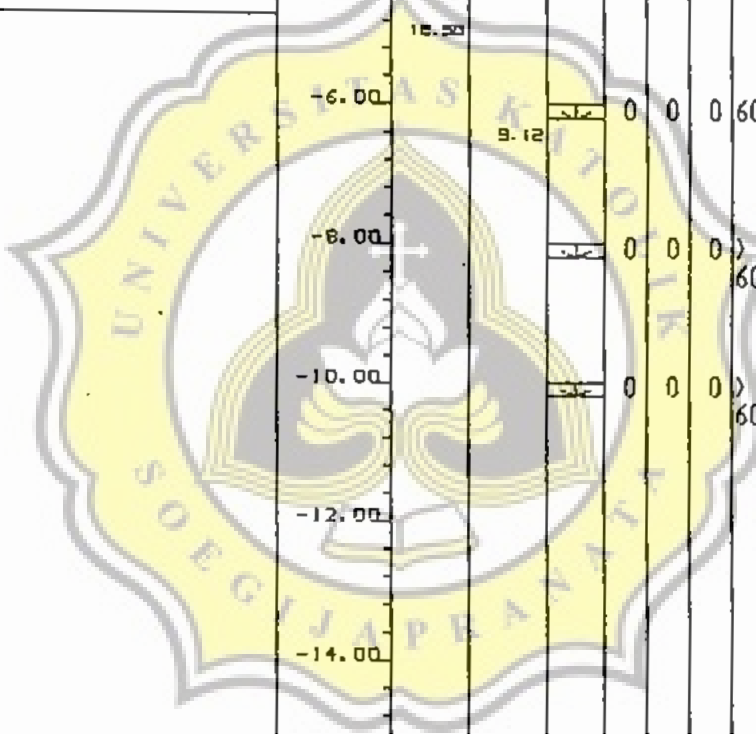
PROJECT : HENRICUS CONSTAN  
 CLIENT : UNIKA  
 LOCATION : PAWIYATAN LUHUR IV/1 - SEMARANG  
 COORD NEZ : ( 0.000, 0.000, 0.000)  
 Job No. : 1

Depth : 10.000  
 Start date : 10/01/97  
 End date : 12/01/97  
 Core Dia : 6  
 Casing Dia : 7.2  
 Driller : unika  
 Logged by : andhi cs

**BORELOG**

HOLE: DB.001

Water	Depth (m)	Core	SOIL/ROCK DESCRIPTION	Elev (m)	US kpa	PP kpa	Remark	SPT Test			
								N-B)ous	N	20 40	
	0		Padas (CR) Padas Warna Coklat	0.00							
	2		Batuan (SS) Batuan Dan Pasir Warna Coklat	-2.00				0	0	0	48
	4		Padas Batuan (RS) Padas Dengan Batuan	-4.00				0	0	0	50
	6			-6.00	15.20			0	0	0	60
	8			-8.00	9.12			0	0	0	60
	10			-10.00				0	0	0	60
	12			-12.00							
	14			-14.00							
	16			-16.00							
	18			-18.00							
	20			-20.00							



10 10%  
 10 20%  
 10 30%  
 10 40%  
 10 50%  
 10 60%  
 10 70%  
 10 80%  
 10 90%  
 10 100%

■ SS - Sand  
 ■ S - Silt  
 ■ GS - Glycer

■ SPT Test  
 ■ Disturbed Sample



**LAB MEKTAN UNIKA SOEGIJAPRANATA**

PROJECT : HENRICUS CONSTAN  
 CLIENT : UNIKA  
 LOCATION : PARIWYATAN LUMUR IV/1 - SEMARANG  
 COORD MEZ : ( 0.000, 0.000, 0.000)  
 Job No. : 2

Depth : 10.000  
 Start date : 13/01/97  
 End date : 18/01/97  
 Core Dia : 6  
 Casing Dia : 7.2  
 Driller : unika  
 Logged by : andhi cs

**BORELOG**

HOLE: DB.002.

Water	Depth (m)	Core	SOIL/ROCK DESCRIPTION	Elev (m)	U S kpa	P P kpa	Remark	SPT Test					
								N-Blows	N	20	40		
	0		Lempung (S) Lempung Padat Warna Coklat	0.00									
	2		Padas Batuan (RS) Padas Dengan Batuan	-2.00			12.58	0	0	0	60		
	4			-4.00			9.12	0	0	0	60		
	6			-6.00				0	0	0	>		
	8			-8.00				0	0	0	>		
	10			-10.00				0	0	0	>		
	12			-12.00									
	14			-14.00									
	16			-16.00									
	18			-18.00									
	20			-20.00									

0 to 10% Trace  UOS - Shelby Tube  SPT Sample  
 10 to 20% Some  UOS - Pison  PMT Test  
 20 to 35% Adjective  UOS - Pitcher  Disturbed Sample  
 35 to 50% And

LAB MEKTAN UNIKA SOEGI JAPRANATA

Job No : 1

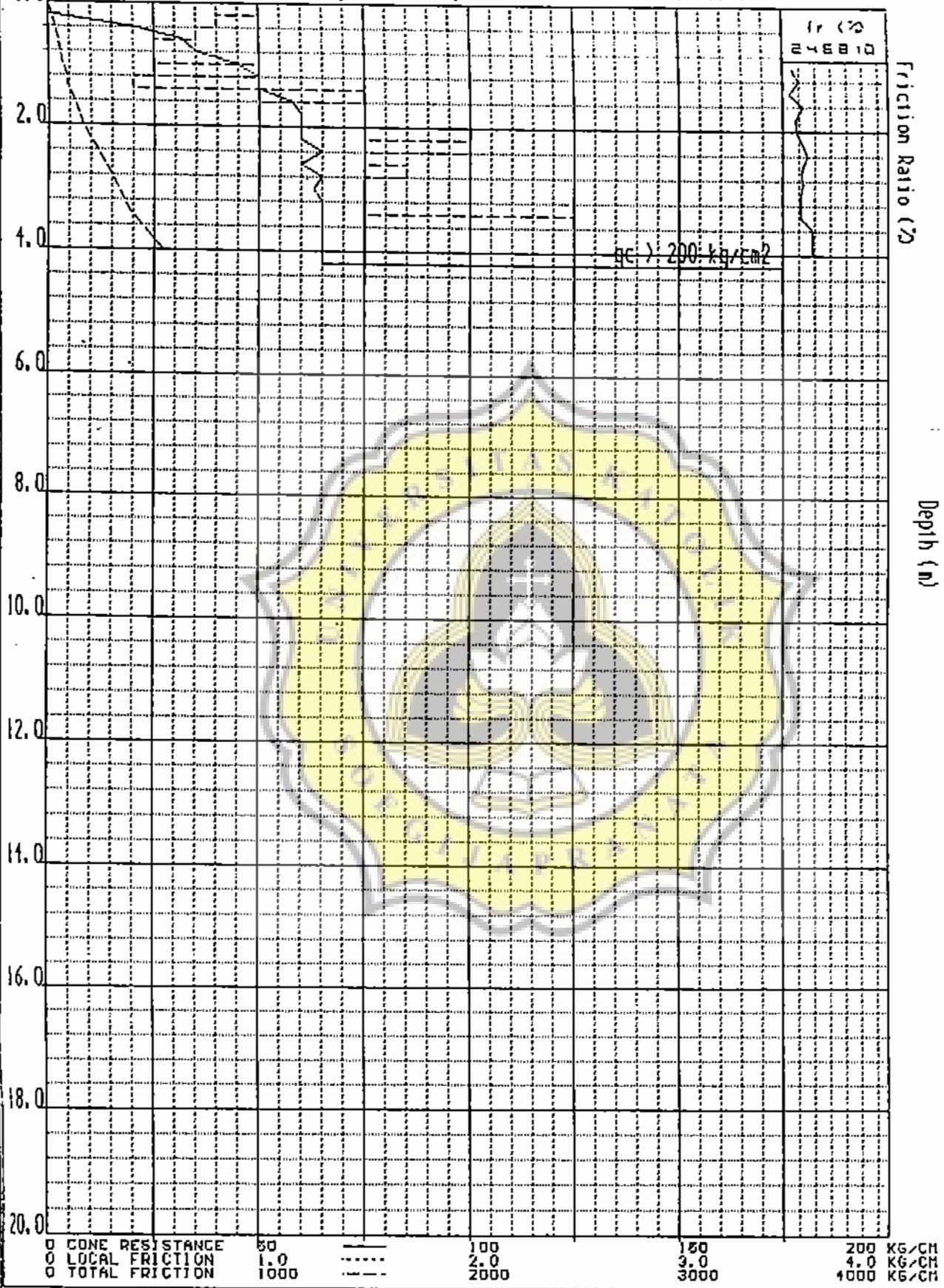
DCPT

Project : HENDRICUS CONSTAN

Point : ST

Test by : Andhi  
Date : 06/01/97

Location: Paviyatan Luhur IQ/1 Semarang



LAB MEKTAN UNIKA SOEGI JAPRANATA

Job No : 2

DCPT

Project : HENDRICUS CONSTAN

Point : S2

Test by : Andhi

Location: Pauriyatan Luhur IV/1 Semarang

Date : 06/01/97

246510

Friction Ratio (%)

Depth (m)

GC : 200 kg/cm<sup>2</sup>

0 CONE RESISTANCE	50	-----	100	150	200 KG/CM <sup>2</sup>
0 LOCAL FRICTION	1.0	-----	2.0	3.0	4.0 KG/CM <sup>2</sup>
0 TOTAL FRICTION	1000	-----	2000	3000	4000 KG/CM <sup>2</sup>

LAB MEKTAN UNIKA SOEGI JAPRANATA

Job No : 3

DCPT

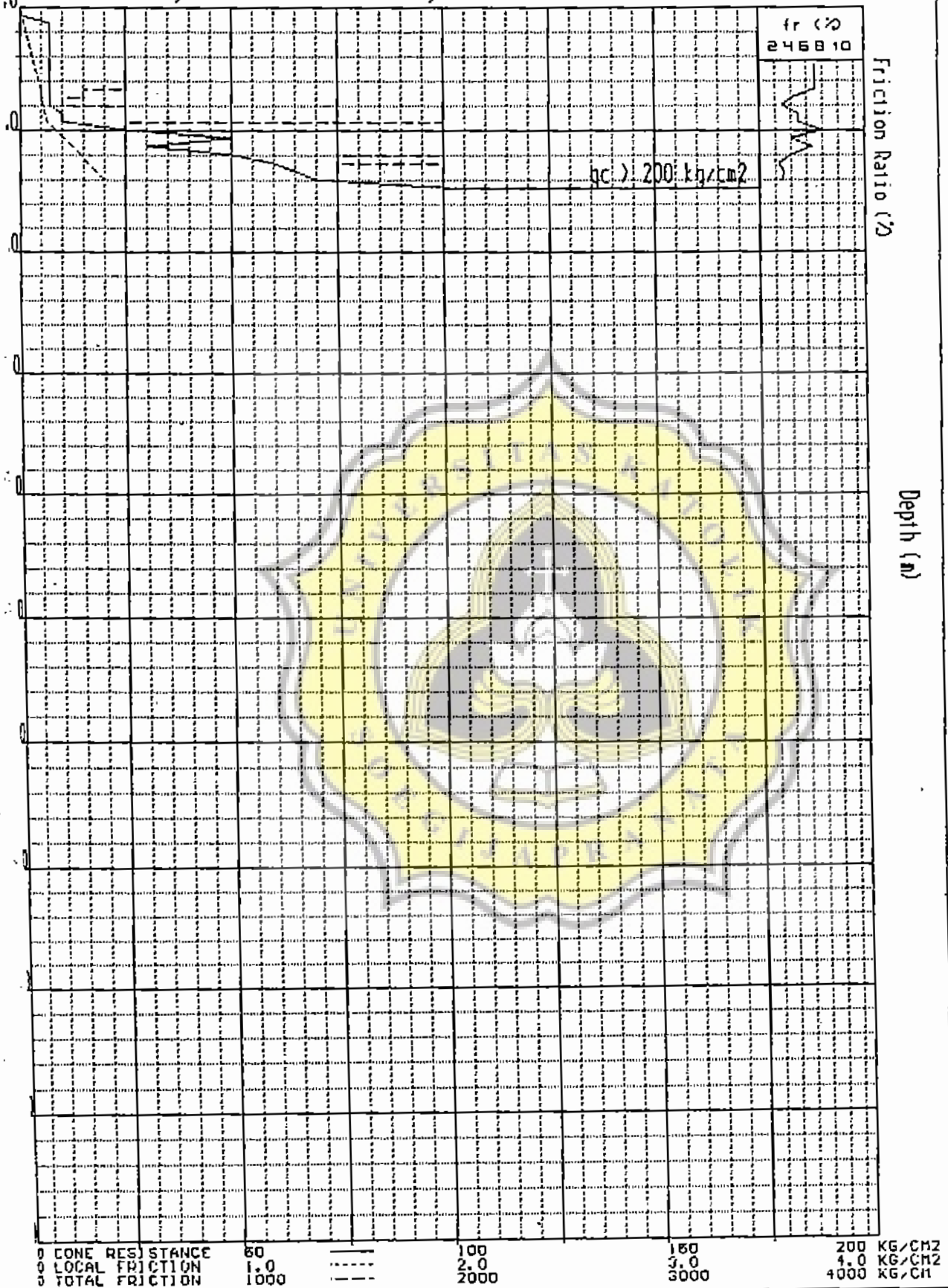
Project : HENDRICUS CONSTAN

Point : S3

Location: Pawiyanan Luhur IV/I Semarang

Test by : Andhi

Date : 06/01/97



LAB MEKTAN UNIKA SOEGI JAPRANATA

Job No : 4

DCPT

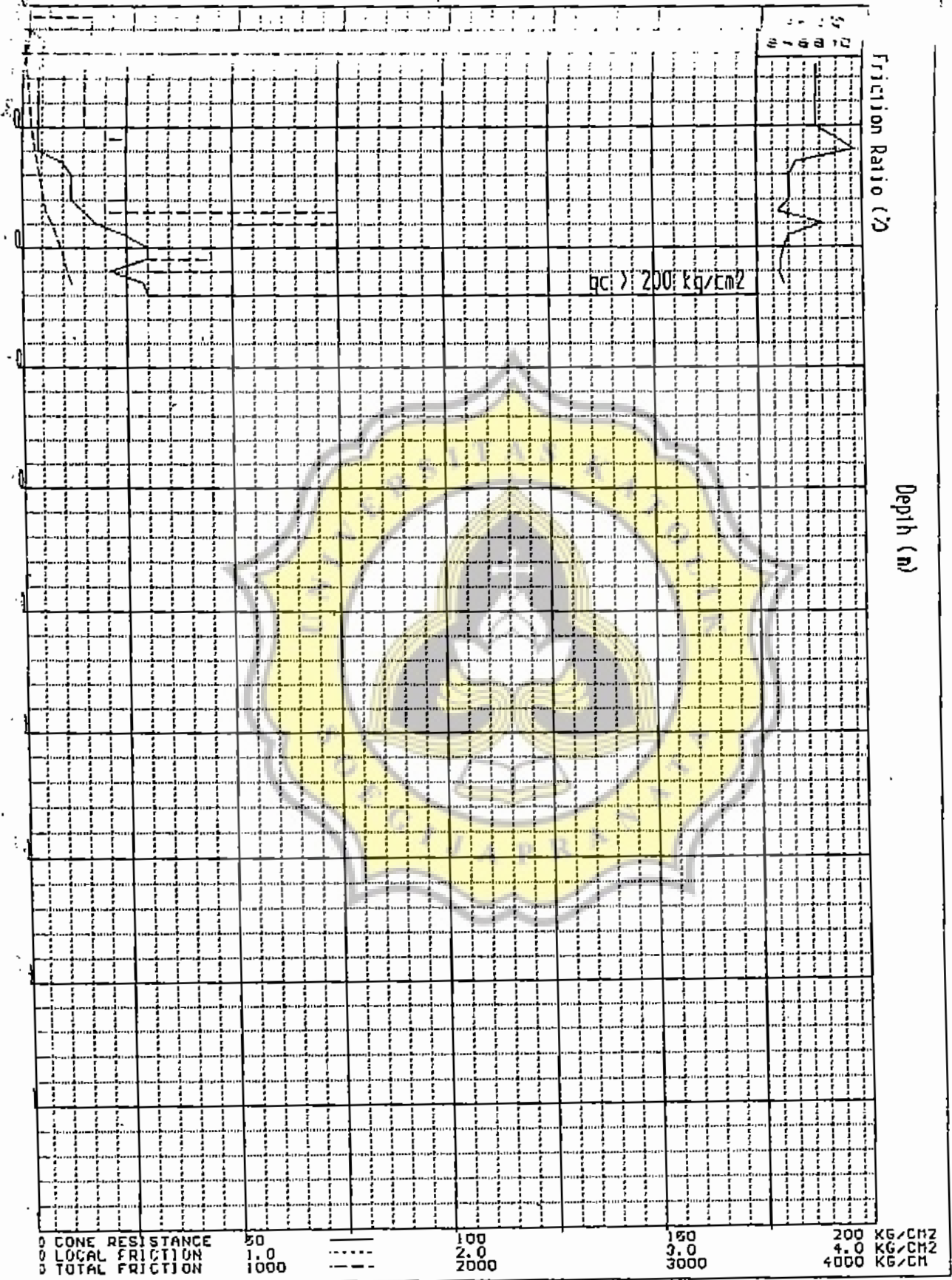
Project : HENDRICUS CONSTAN

Point : S4

Test by : Andhi

Location: Gedung an Luber 202 Semarang

Date : 06.03.97



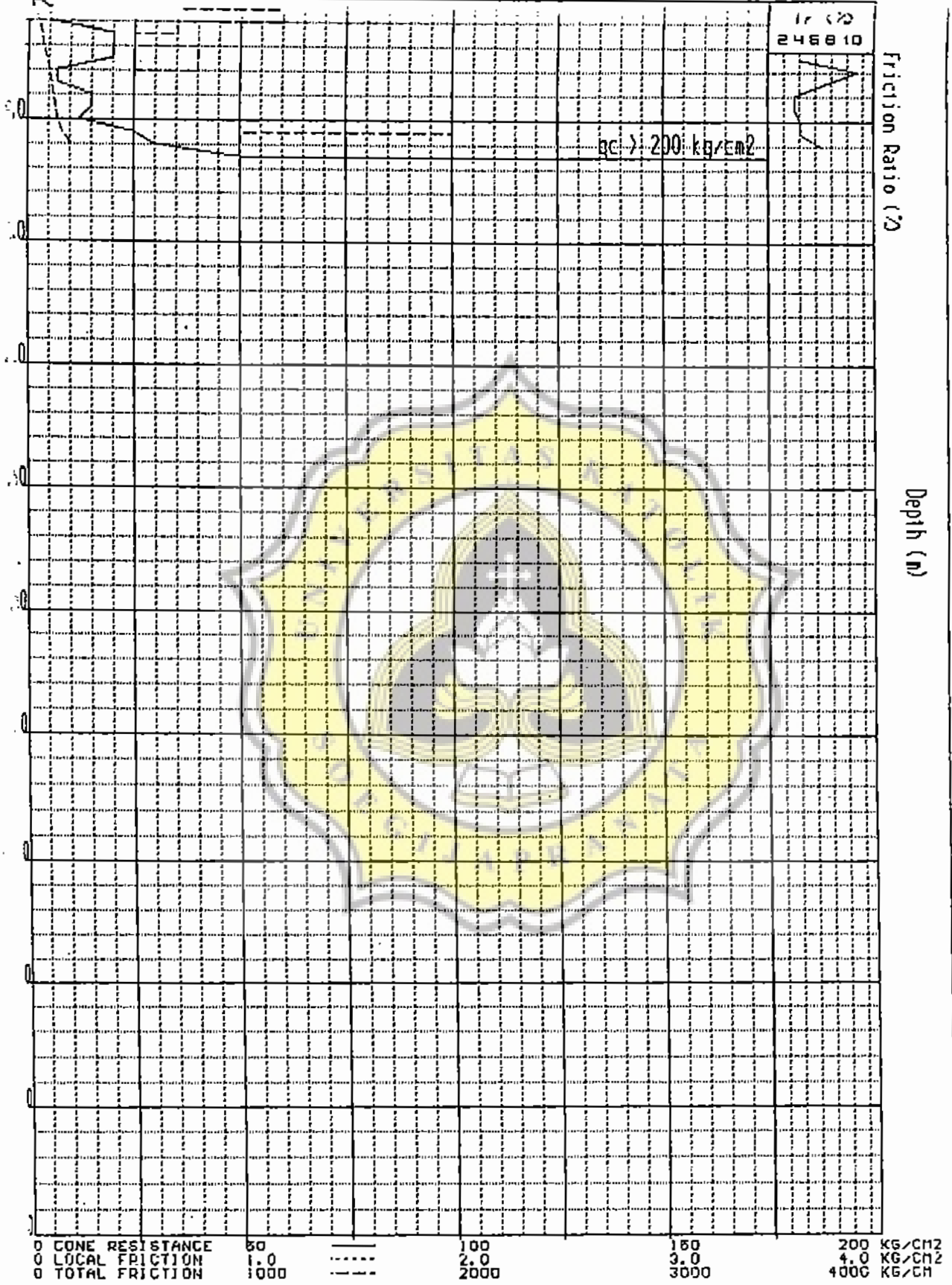
LAB MEKTAN UNIKA SOEGI JAPRANATA Job No : 5

DCPT

Project : HENDRICUS CONSTAN

Date :

Time :



LAB MEKTAN UNIKA SOEGI JAPRANATA

Job No : 6

DCPT

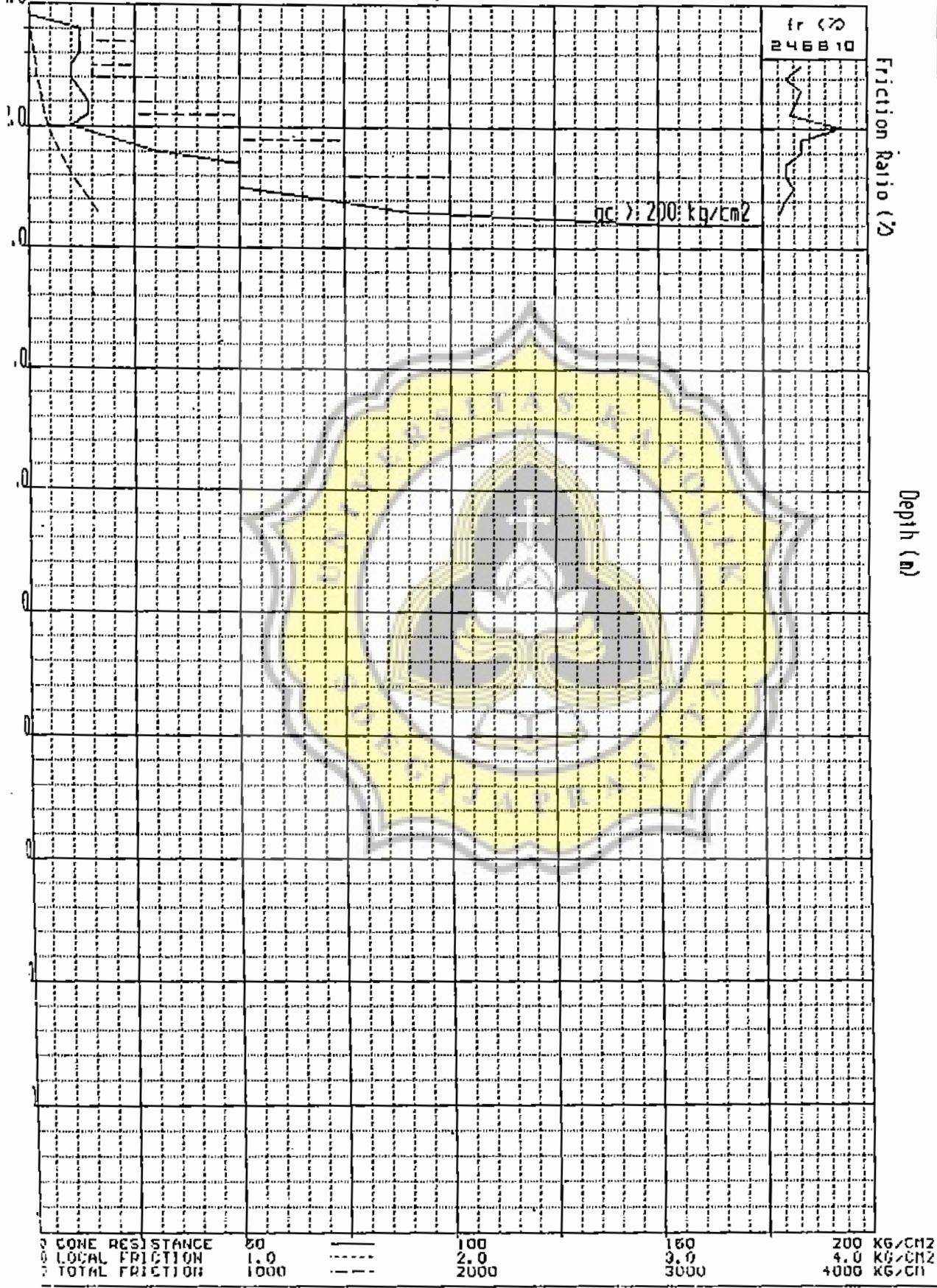
Project : HENDRICUS CONSTAN

Point : S6

Test by : Andhi

Date : 06/01/97

Location: Paviyatan Luhur IV/1 Semarang



LAB MEKTAN UNIKA SOEGI JAPRANATA

Job No : 7

DCPT

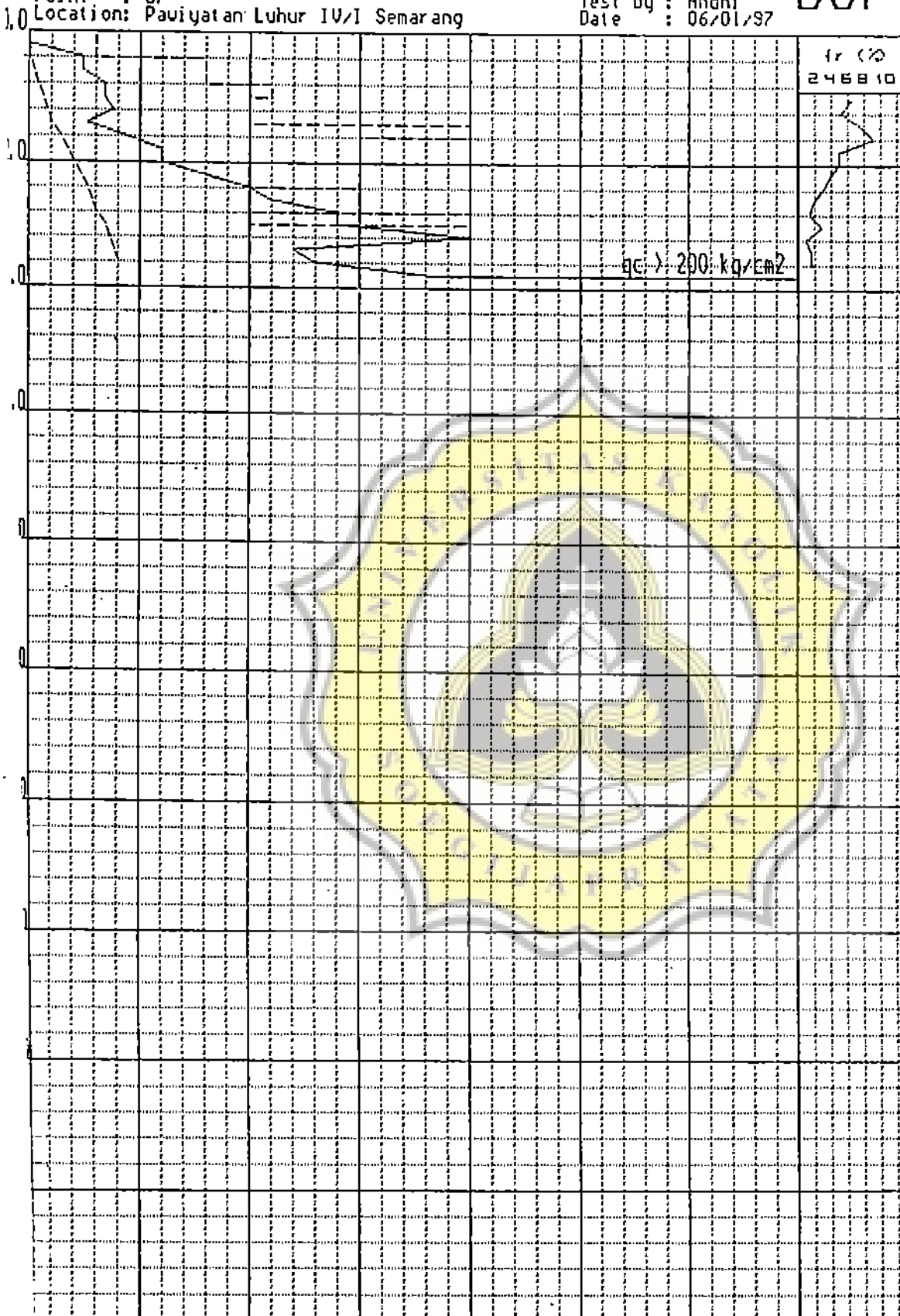
Project : HENDRICUS CONSTAN

Point : S7

Location: Pantiyatan Luhur IV/I Semarang

Test by : Andhi

Date : 06/01/97



Friction Ratio (%)

Depth (m)

1) CONE RESISTANCE	50	-----	100	150	200 KG/CM <sup>2</sup>
2) LOCAL FRICTION	1.0	-----	2.0	3.0	4.0 KG/CM <sup>2</sup>
3) TOTAL FRICTION	1000	-----	2000	3000	4000 KG/CM <sup>2</sup>





**LABORATORIUM MEKANIKA TANAH**  
**UNIVERSITAS KATOLIK SOEGIJAPRANATA**

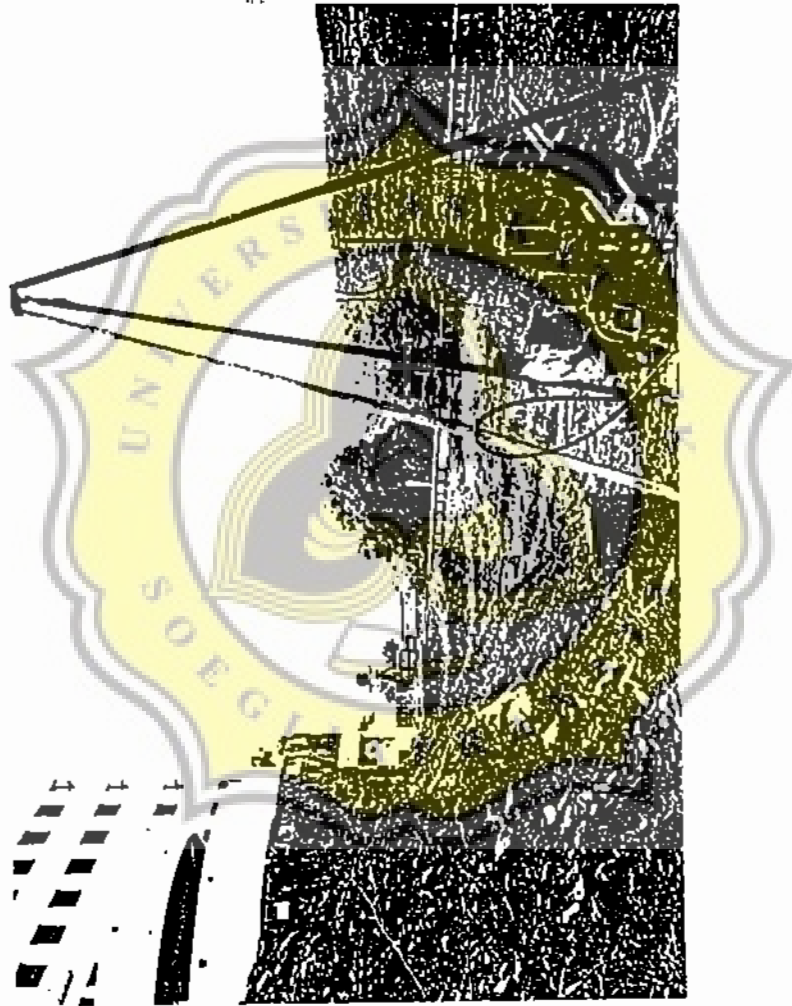
Jl. Pawiyatan Luhur IV / 1 Bendan Dhuwur Semarang - 50234

Telp. (024) 316142 - 441555 (Hunting)

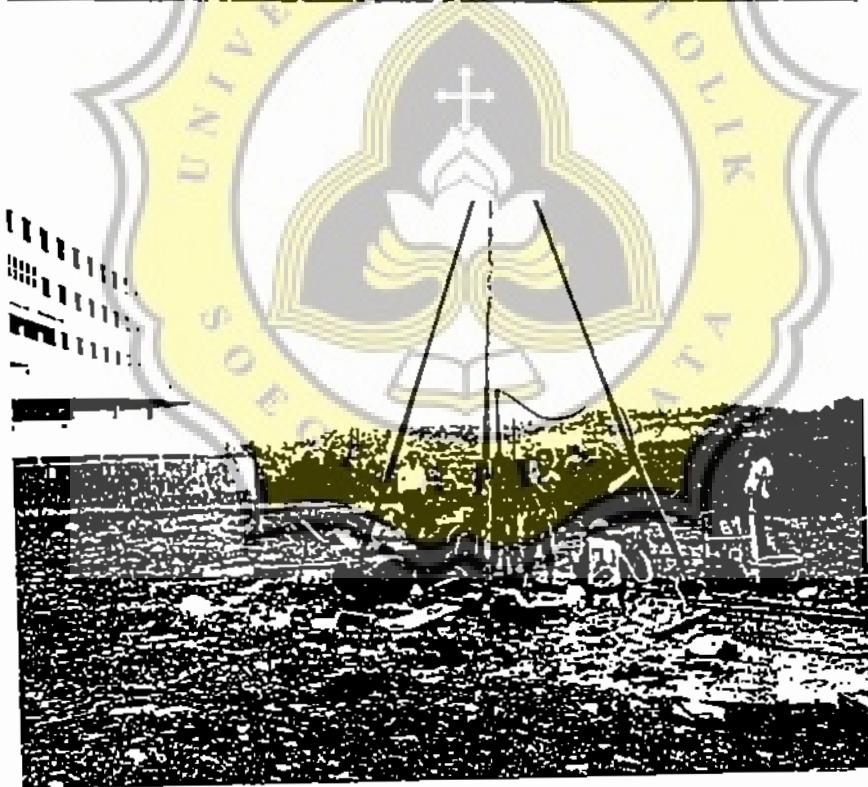
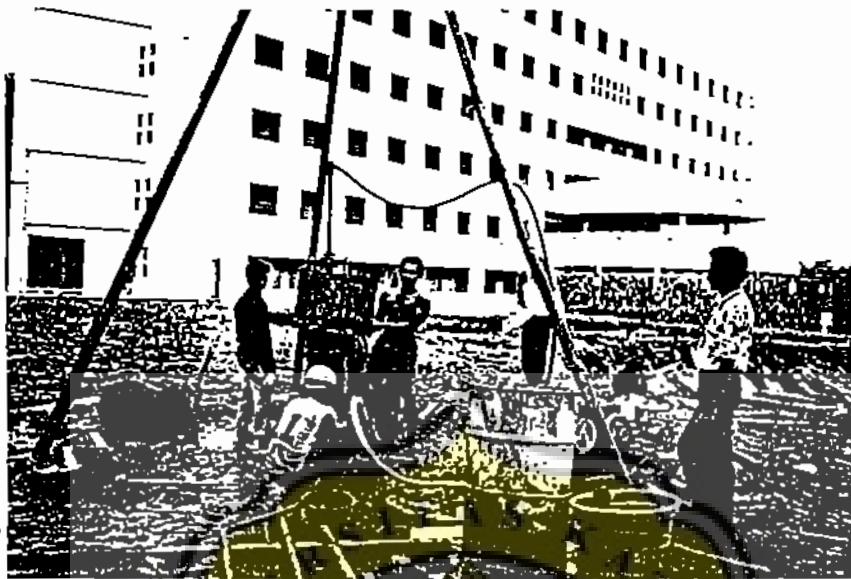
Fax. (024) 415429 E-Mail : [unika@semarang.wasantara.net.id](mailto:unika@semarang.wasantara.net.id). Po. Box. 8033/S.I

Badan Hukum : Yayasan Sandjojo

---









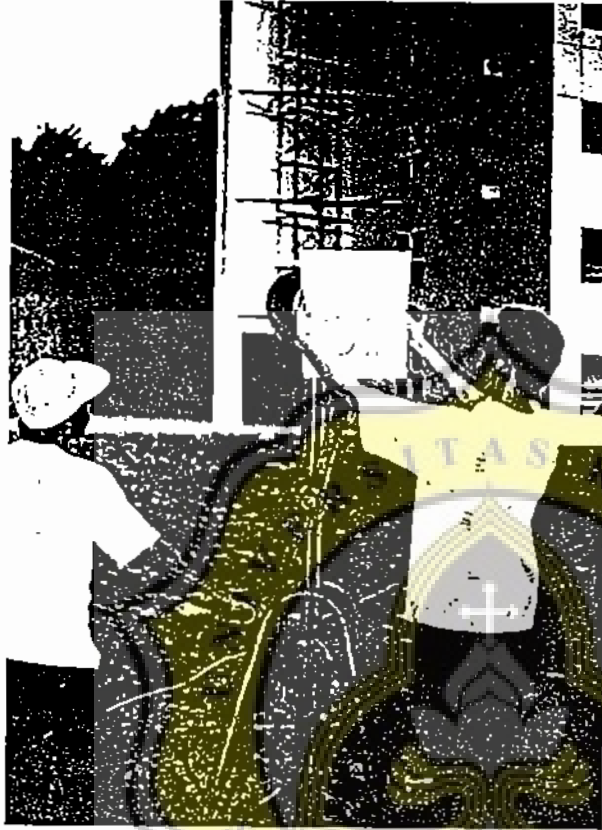
**LABORATORIUM MEKANIKA TANAH**  
**UNIVERSITAS KATOLIK SOEGIJAPRANATA**

Jl. Pawiyatan Luhur IV / 1 Bendan Dhuwur Semarang - 50234

Telp. (024) 316142 - 441555 (Hunting)

Fax. (024) 415429 E-Mail : unika@semarang.wasantara.net.id. Po. Box. 8033/SI.1

Badan Hukum : Yayasan Sandjojo





**LABORATORIUM MEKANIKA TANAH**  
**UNIVERSITAS KATOLIK SOEGIJAPRANATA**

Jl. Pawiyatan Luhur IV / 1 Bendan Dhuwur Semarang - 50234

Telp. (024) 316142 - 441555 (Hunting)

Fax. (024) 415429 E-Mail : [unika@semarang.wasantara.net.id](mailto:unika@semarang.wasantara.net.id). Po. Box. 8033/SM

Badan Hukum : Yayasan Sandjojo





**LABORATORIUM MEKANIKA TANAH**  
**UNIVERSITAS KATOLIK SOEGIJAPRANATA**

Jl. Pawiyatan Luhur IV / 1 Bendan Dhuwur Semarang - 50234

Telp. (024) 316142 - 441555 (Hunting)

Fax. (024) 415429 E-Mail : [unika@semarang.wasantara.net.id](mailto:unika@semarang.wasantara.net.id). Po. Box. 8033/SM

Badan Hukum : Yayasan Sandjojo





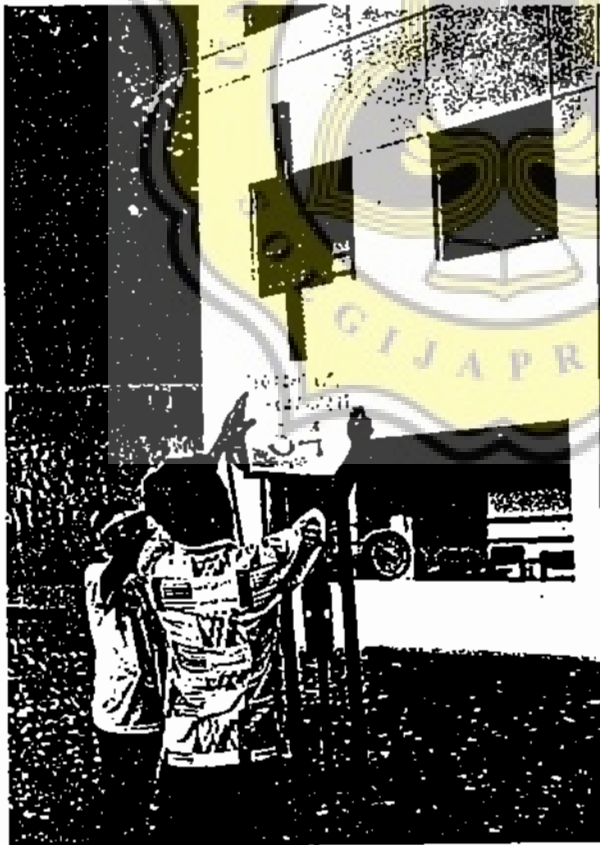
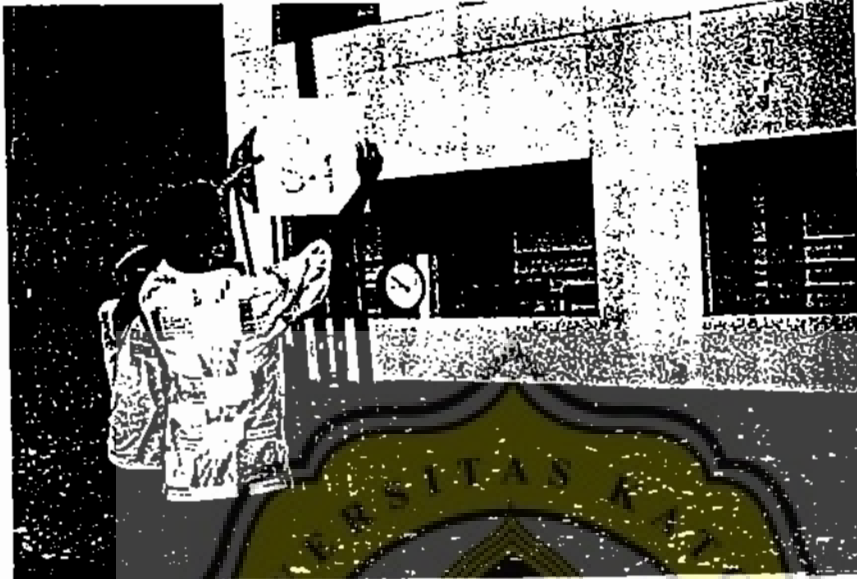
**LABORATORIUM MEKANIKA TANAH**  
**UNIVERSITAS KATOLIK SOEGIJAPRANATA**

Jl. Pawiyatan Luhur IV / 1 Bendan Dhuwur Semarang - 50234

Telp. (024) 316142 - 441555 (Hunting)

Fax. (024) 415429 E-Mail : unika@semarang.wasantara.net.id. Po. Box. 8033/SM

Badan Hukum : Yayasan Sandjojo





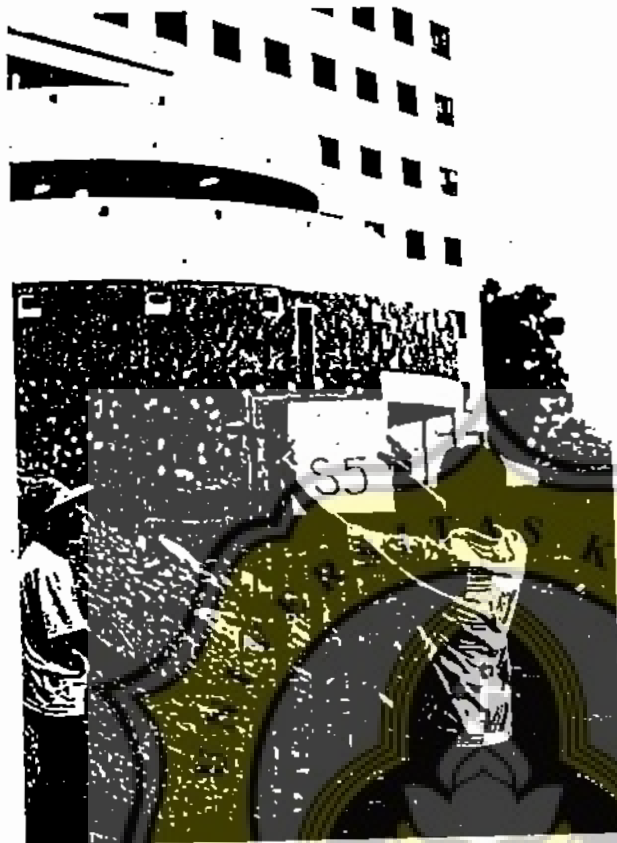
**LABORATORIUM MEKANIKA TANAH  
UNIVERSITAS KATOLIK SOEGIJAPRANATA**

Jl. Pawiyatan Luhur IV / 1 Bendan Dhuwur Semarang - 50234

Telp. (024) 316142 - 441555 (Hunting)

Fax. (024) 415429 E-Mail : [unika@semarang.wasantara.net.id](mailto:unika@semarang.wasantara.net.id). Po. Box. 8033/SM

Badan Hukum : Yayasan Sandjojo







**LABORATORIUM MEKANIKA TANAH**  
**UNIVERSITAS KATOLIK SOEGIJAPRANATA**

Jl. Pawiyatan Luhur IV / 1 Bendan Dhuwur Semarang - 50234

Telp. (024) 316142 - 441555 (Hunting)

Fax. (024) 415429 E-Mail : [unika@semarang.wasantara.net.id](mailto:unika@semarang.wasantara.net.id). Po. Box. 8033/SM

Badan Hukum : Yayasan Sandjojo





**LABORATORIUM MEKANIKA TANAH**  
**UNIVERSITAS KATOLIK SOEGIJAPRANATA**

Jl. Pawiyatan Luhur IV / 1 Bendan Dhuwur Semarang - 50234

Telp. (024) 316142 - 441555 (Hunting)

Fax. (024) 415429 E-Mail : [unika@semarang.wasantara.net.id](mailto:unika@semarang.wasantara.net.id). Po. Box. 8033/SM

Badan Hukum : Yayasan Sandjojo



LAMPIRAN IX.  
 TABEL UNTUK CARA KEKUATAN BATAS  
 ( oleh ir. Wiratman )  
 $\delta = 0$

$\alpha$	$\xi_u$	$\sigma_u$	$\sigma_u'$	$\xi$	$q$	$C_u$
.055	.069	13.545	0	.972	.0275	6.12
.058	.073	12.793	0	.971	.029	5.96
.06	.075	12.333	0	.97	.03	5.86
.063	.079	11.698	0	.969	.0315	5.72
.065	.081	11.308	0	.968	.0325	5.64
.068	.085	10.765	0	.966	.034	5.52
.07	.088	10.429	0	.965	.035	5.44
.073	.091	9.959	0	.954	.0365	5.33
.075	.094	9.667	0	.962	.0375	5.26
.078	.097	9.256	0	.961	.039	5.17
.08	.1	9.0	0	.96	.04	5.1
.083	.104	8.639	0	.959	.0415	5.01
.085	.106	8.412	0	.958	.0425	4.96
.088	.11	8.091	0	.956	.044	4.88
.090	.112	7.889	0	.955	.045	4.82
.093	.116	7.602	0	.954	.0465	4.75
.095	.119	7.421	0	.952	.0475	4.7
.098	.122	7.163	0	.951	.049	4.63
.100	.125	7.0	0	.95	.05	4.59
.103	.129	6.767	0	.949	.0515	4.52
.105	.131	6.619	0	.948	.0525	4.48
.108	.135	6.407	0	.946	.054	4.42
.110	.138	6.273	0	.945	.055	4.39
.113	.141	6.08	0	.944	.0565	4.33
.115	.144	5.957	0	.943	.0575	4.29
.118	.148	5.78	0	.941	.059	4.24
.120	.150	5.667	0	.94	.06	4.21
.123	.154	5.504	0	.939	.0615	4.16
.125	.156	5.4	0	.938	.0625	4.13
.128	.16	5.25	0	.936	.064	4.09
.130	.163	5.154	0	.935	.065	4.06
.133	.166	5.015	0	.934	.0665	4.01
.135	.169	4.926	0	.933	.0675	3.98
.138	.173	4797	0	.931	.069	3.95
.140	.175	4.714	0	.930	.070	3.92
.143	.179	4.594	0	.929	.0715	3.88
.145	.181	4.517	0	.928	.0725	3.86
.147	.185	4.405	0	.926	.074	3.82
.150	.188	4.333	0	.925	.075	3.8
.153	.191	4.229	0	.924	.0765	3.76
.155	.194	4.161	0	.923	.0775	3.74
.158	.198	4.063	0	.921	.079	3.71
.160	.20	4.0	0	.920	.080	3.69
.163	.204	3.908	0	.918	.0815	3.66
.165	.206	3.848	0	.918	.0825	3.63
.168	.21	3.762	0	.916	.084	3.61
.170	.213	3.706	0	.915	.085	3.69
.173	.216	3.624	0	.914	.0865	3.56
.175	.219	3.571	0	.913	.0875	3.54
.178	.2220	3.494	0	.911	.089	3.51
.180	.225	3.444	0	.910	.090	3.49
.185	.229	3.372	0	.909	.0915	3.47
.185	.231	3.324	0	.908	.0925	3.45

$\delta = 0$

$\alpha$	$F_u$	$\sigma_u$	$\sigma_u'$	$F_u$	q	Cu
.188	.235	3.255	0	.906	.094	3.43
.190	.238	3.211	0	.905	.095	3.41
.193	.241	3.145	0	.904	.0965	3.39
.195	.244	3.103	0	.903	.0975	3.37
.198	.248	3.04	0	.901	.099	3.35
.200	.250	3	0	.90	.10	3.33
.203	.254	2.941	0	.899	.1015	3.31
.205	.25	2.912	0	.898	.1025	3.3
.208	.26	2.846	0	.896	.1040	3.28
.21	.262	2.81	0	.895	.105	3.26
.213	.266	2.756	0	.894	.1065	3.24
.215	.269	2.721	0	.893	.1075	3.23
.218	.272	2.67	0	.891	.109	3.21
.220	.275	2.636	0	.890	.110	3.2
.223	.279	2.587	0	.889	.1115	3.18
.225	.281	2.556	0	.888	.1125	3.16
.228	.285	2.509	0	.886	.114	3.15
.230	.287	2.478	0	.885	.115	3.13
.233	.291	2.433	0	.884	.1165	3.12
.235	.294	2.404	0	.883	.1175	3.1
.238	.297	2.361	0	.881	.119	3.09
.240	.300	2.333	0	.880	.120	3.08
.243	.304	2.292	0	.879	.1215	3.06
.245	.306	2.265	0	.878	.1225	3.05
.248	.310	2.226	0	.876	.124	3.03
.250	.312	2.200	0	.876	.125	3.02
.253	.316	2.162	0	.874	.1265	3.01
.255	.319	2.137	0	.873	.1275	3.0
.258	.322	2.101	0	.871	.129	2.98
.260	.325	2.077	0	.870	.130	2.97
.263	.329	2.042	0	.869	.1315	2.96
.265	.331	2.019	0	.868	.1325	2.95
.268	.335	1.985	0	.866	.134	2.94
.270	.337	1.963	0	.865	.135	2.93
.273	.341	1.930	0	.864	.1365	2.91
.275	.344	1.909	0	.863	.1375	2.90
.278	.347	1.878	0	.861	.139	2.89
.280	.35	1.857	0	.86	.14	2.88
.283	.354	1.827	0	.859	.1415	2.87
.285	.336	1.807	0	.858	.1425	2.86
.288	.36	1.778	0	.856	.144	2.85
.290	.363	1.759	0	.855	.145	2.84
.293	.366	1.73	0	.854	.1465	2.83
.295	.369	1.712	0	.853	.1475	2.82
.298	.372	1.685	0	.851	.149	2.81
.300	.375	1.667	0	.850	.150	2.800
.303	.379	1.64	0	.849	.1515	2.79
.305	.381	1.623	0	.848	.1525	2.78
.308	.385	1.597	0	.846	.154	2.77
.310	.387	1.581	0	.845	.155	2.76
.313	.391	1.556	0	.844	.1565	2.75
.315	.394	1.54	0	.843	.1575	2.74
.318	.397	1.516	0	.841	.159	2.73
.320	.4	1.5	0	.84	.16	2.73
.323	.404	1.477	0	.839	.1615	2.72
.325	.406	1.462	0	.838	.1625	2.71
.328	.41	1.439	0	.836	.164	2.7

$$\delta = 0$$

$\alpha$	$F_u$	$\theta_u$	$\theta_u'$	$F_u$	$q$	$C_u$
.330	.412	1.424	0	.835	.165	2.69
.333	.416	1.402	0	.834	.1665	2.68
.335	.419	1.388	0	.833	.1675	2.68
.338	.422	1.367	0	.831	.169	2.67
.340	.425	1.353	0	.830	.170	2.66
.342	.429	1.332	0	.829	.1715	2.65
.345	.431	1.319	0	.828	.1725	2.65
.348	.435	1.299	0	.826	.174	2.64
.350	.437	1.286	0	.825	.175	2.65
.353	.441	1.266	0	.824	.1765	2.62
.355	.444	1.254	0	.823	.1775	2.62
.358	.447	1.235	0	.821	.179	2.61
.36	.45	1.222	0	.820	.180	2.60
.363	.454	1.204	0	.819	.1815	2.59
.365	.456	1.192	0	.818	.1825	2.59
.368	.460	1.174	0	.816	.184	2.58
.370	.462	1.162	0	.815	.185	2.58
.373	.466	1.145	0	.814	.1865	2.57
.375	.469	1.133	0	.813	.1875	2.56
.378	.472	1.116	0	.811	.189	2.55
.380	.475	1.105	0	.81	.19	2.55
.383	.479	1.089	0	.809	.1915	2.54
.385	.481	1.078	0	.808	.1925	2.54
.388	.485	1.062	0	.806	.194	2.53
.390	.488	1.051	0	.805	.195	2.52
.393	.491	1.036	0	.804	.1965	2.52
.395	.494	1.025	0	.803	.1975	2.51
.398	.497	1.01	0	.801	.199	2.51
.400	.500	1.0	0	.800	.200	2.50
.403	.504	.985	0	.799	.2015	2.49
.405	.506	.975	0	.798	.2025	2.49
.408	.510	.961	0	.796	.204	2.48
.410	.513	.951	0	.795	.205	2.48
.413	.516	.937	0	.794	.2065	2.47
.415	.519	.928	0	.793	.2075	2.47
.418	.523	.914	0	.791	.209	2.46
.420	.525	.905	0	.790	.210	2.46
.423	.529	.891	0	.789	.2115	2.45
.425	.531	.882	0	.788	.2125	2.44
.428	.535	.869	0	.786	.214	2.44
.430	.538	.860	0	.785	.215	2.43
.433	.541	.848	0	.784	.2165	2.43
.435	.544	.839	0	.783	.2175	2.42
.438	.547	.826	0	.781	.219	2.42
.440	.550	.818	0	.780	.220	2.41
.443	.554	.806	0	.779	.2215	2.41
.445	.556	.798	0	.778	.2225	2.40
.448	.560	.786	0	.776	.224	2.40
.450	.563	.778	0	.775	.225	2.39
.453	.566	.766	0	.774	.2265	2.39
.455	.569	.758	0	.773	.2275	2.38
.458	.573	.747	0	.771	.229	2.38
.460	.575	.739	0	.770	.230	2.38
.465	.579	.728	0	.769	.2315	2.37
.465	.581	.720	0	.768	.2325	2.37
.468	.585	.709	0	.766	.234	2.36
.470	.587	.702	0	.765	.235	2.36
.473	.591	.691	0	.764	.2365	2.35

$\delta=0$

$\alpha$	$\xi_u$	$\theta_u$	$\theta_u'$	$\xi$	$q$	$C_u$
.478	.597	.674	0	.761	.239	2.34
.480	.600	.667	0	.76	.24	2.34
.483	.604	.656	0	.759	.2415	2.34
.485	.606	.649	0	.758	.2425	2.33
.488	.610	.639	0	.756	.244	2.33
.490	.613	.633	0	.755	.245	2.33
.493	.616	.623	0	.754	.2465	2.32
.495	.619	.616	0	.753	.2475	2.32
.498	.623	.606	0	.751	.249	2.31
.500	.625	.600	0	.750	.250	2.31
.530	.663	.509	0	.735	.265	2.27
.550	.688	.455	0	.725	.275	2.24

$\delta=0,2$

$\alpha$	$\xi_u$	$\theta_u$	$\theta_u'$	$\xi$	$q$	$C_u$
.055	.069	13.545	-.455	.958	.03437	5.51
.058	.073	12.793	-.379	.957	.03625	5.37
.060	.075	12.3333	-.333	.956	.0375	5.28
.063	.078	11.698	-.27	.955	.03938	5.16
.065	.081	11.308	-.231	.954	.04062	5.08
.068	.085	10.765	-.176	.953	.0425	4.97
.070	.088	10.429	-.143	.952	.04375	4.90
.073	.091	9.959	-.096	.951	.04562	4.8
.075	.094	9.667	-.067	.950	.04687	4.74
.078	.097	9.256	-.026	.949	.04875	4.65
.080	.100	9.0	0	.948	.05	4.59
.083	.104	8.639	.036	.947	.05187	4.51
.085	.106	8.412	.059	.946	.05313	4.46
.088	.110	8.091	.091	.945	.055	4.39
.090	.112	7.889	.111	.944	.05625	4.34
.093	.116	7.602	.140	.943	.05813	4.27
.095	.119	7.421	.158	.942	.05937	4.23
.098	.122	7.163	.184	.941	.06125	4.17
.100	.125	7.0	.200	.940	.0625	4.13
.103	.129	6.767	.223	.939	.06438	4.07
.105	.131	6.619	.238	.938	.06562	4.03
.108	.135	6.407	.259	.937	.0675	3.98
.110	.138	6.273	.273	.936	.06875	3.94
.113	.141	6.08	.292	.935	.07063	3.89
.115	.144	5.957	.304	.934	.07188	3.86
.118	.148	5.78	.322	.933	.07375	3.81
.120	.150	5.667	.333	.932	.075	3.78
.123	.154	5.504	.350	.931	.07688	3.74
.125	.156	5.400	.360	.930	.07813	3.71
.128	.160	525	.375	.929	.080	3.67
.130	.163	5.154	.385	.928	.08125	3.64
.133	.166	5.015	.398	.927	.08313	3.60
.135	.169	4.926	.407	.926	.08438	3.58
.138	.173	4.797	.420	.925	.08625	3.54
.140	.175	4.714	.429	.924	.0875	3.52
.143	.179	4.594	.441	.923	.08938	3.48
.145	.181	4.517	.448	.922	.09063	3.46
.148	.185	4.405	.459	.921	.0925	3.43
.150	.188	4.333	.467	.920	.09375	3.41
.153	.191	4.229	.477	.919	.09563	3.37

$$\delta = 0,2$$

$\alpha$	$F_u$	$\sigma_u$	$\sigma_u'$	$\xi$	$q$	$C_u$
.155	.194	4.161	.484	.918	.09687	3.35
.158	.198	4.063	.494	.917	.09875	3.32
.160	.200	4.0	.500	.916	.100	3.30
.163	.204	3.908	.509	.915	.10188	3.28
.163	.206	3.848	.515	.914	.10313	3.26
.168	.210	3.762	.524	.913	.105	3.23
.170	.213	3.706	.529	.912	.10625	3.21
.173	.216	3.624	.538	.911	.10812	3.19
.175	.219	3.571	.564	.910	.10938	3.17
.178	.222	3.494	.551	.909	.11125	3.14
.180	.225	3.444	.556	.908	.1125	3.13
.183	.229	3.372	.563	.907	.11437	3.10
.185	.231	3.325	.568	.906	.11563	3.09
.188	.235	3.255	.574	.905	.1175	3.07
.190	.238	3.211	.579	.904	.11875	3.05
.193	.241	3.145	.585	.903	.12062	3.03
.195	.244	3.103	.590	.902	.12188	3.02
.198	.248	3.04	.596	.901	.12375	2.99
.200	.250	3.0	.600	.900	.125	2.98
.203	.254	2.941	.606	.899	.12687	2.96
.205	.256	2.902	.610	.898	.12687	2.95
.208	.260	2.846	.615	.897	.130	2.93
.210	.262	2.81	.619	.896	.13125	2.92
.213	.266	2.756	.624	.895	.13312	2.90
.215	.269	2.721	.628	.894	.13438	2.89
.218	.272	2.67	.633	.893	.13625	2.87
.220	.275	2.636	.636	.892	.1375	2.86
.223	.279	2.587	.641	.891	.13937	2.84
.225	.281	2.556	.644	.890	.14062	2.83
.228	.285	2.509	.649	.889	.1425	2.81
.230	.287	2.478	.652	.888	.14375	2.80
.233	.291	2.433	.657	.887	.14562	2.78
.235	.294	2.404	.660	.886	.14687	2.77
.238	.297	2.361	.664	.885	.14875	2.76
.240	.300	2.333	.667	.884	.150	2.75
.243	.304	2.292	.671	.883	.15187	2.73
.243	.306	2.265	.673	.882	.15312	2.72
.248	.310	2.226	.677	.881	.155	2.71
.250	.312	2.2	.68	.88	.15625	2.70
.253	.316	2.162	.684	.879	.15812	2.68
.255	.319	2.137	.686	.878	.15937	2.67
.258	.322	2.101	.690	.877	.16125	2.66
.260	.325	2.077	.692	.876	.1625	2.65
.263	.329	2.042	.696	.875	.16437	2.64
.265	.331	2.019	.698	.874	.16563	2.63
.268	.335	1.985	.701	.873	.1675	2.62
.270	.337	1.963	.704	.872	.16865	2.61
.273	.341	1.930	.707	.871	.17062	2.59
.275	.344	1.909	.709	.870	.17187	2.59
.278	.347	1.878	.712	.869	.17375	2.57
.280	.350	1.857	.714	.868	.175	2.57
.285	.357	1.827	.717	.867	.17687	2.55
.285	.356	1.807	.719	.866	.17812	2.55
.288	.360	1.778	.722	.865	.180	2.53
.290	.363	1.759	.724	.864	.18125	2.53





$\delta = 0,2$

Cu	$\alpha$	$\xi_u$	$\rho_u$	$\rho_u'$	$\xi$	q	Cu
2.52	.430	.538	.860	.814	.808	.26875	2.15
2.51	.433	.541	.848	.815	.807	.27063	2.14
2.50	.435	.544	.837	.816	.806	.27188	2.14
2.49	.438	.547	.826	.817	.805	.27375	2.13
2.48	.440	.550	.818	.818	.804	.2750	2.13
2.47	.443	.554	.806	.819	.803	.27688	2.12
2.46	.448	.560	.786	.821	.801	.280	2.11
2.46	.450	.563	.778	.822	.800	.28125	2.11
2.45	.453	.566	.766	.823	.799	.28312	2.10
2.44	.455	.569	.758	.824	.798	.28438	2.10
2.43	.458	.573	.747	.825	.797	.28625	2.09
2.42	.460	.575	.739	.826	.796	.2875	2.09
2.41	.463	.579	.728	.827	.795	.28937	2.08
2.41	.465	.581	.720	.828	.794	.29063	2.08
2.400	.46	.585	.709	.829	.793	.2925	2.08
2.39	.47	.587	.702	.830	.792	.29375	2.07
2.38	.473	.591	.691	.831	.791	.29563	2.07
2.38	.478	.597	.674	.833	.789	.29875	2.06
2.37	.480	.600	.667	.833	.788	.300	2.06
2.36	.483	.604	.656	.834	.787	.30188	2.05
2.35	.485	.606	.649	.835	.786	.30313	2.05
2.35	.488	.610	.639	.836	.785	.305	2.04
2.34	.490	.613	.633	.837	.784	.30625	2.04
2.33	.493	.616	.623	.838	.783	.30813	2.04
2.32	.495	.619	.616	.838	.782	.30937	2.03
2.32	.498	.623	.606	.839	.781	.31125	2.03
2.31	.500	.625	.600	.840	.780	.3125	2.03
2.31	.530	.663	.509	.849	.768	.33125	1.98
2.30	.550	.688	.455	.855	.760	.344375	1.96

$\delta = 0,4$

Cu	$\alpha$	$\xi_u$	$\rho_u$	$\rho_u'$	$\xi$	q	Cu
2.27	.055	.069	13.545	-.455	.944	.04583	4.81
2.26	.058	.073	12.793	-.379	.943	.04833	4.68
2.25	.060	.075	12.333	-.333	.942	.050	4.61
2.24	.063	.079	11.698	-.27	.941	.0525	4.50
2.23	.065	.081	11.308	-.231	.941	.05417	4.43
2.22	.068	.085	10.765	-.176	.940	.05667	4.33
2.22	.070	.088	10.429	-.143	.939	.05833	4.27
2.21	.073	.091	9.959	-.096	.935	.06083	4.19
2.21	.075	.094	9.667	-.087	.938	.0625	4.13
2.20	.078	.097	9.256	-.026	.937	.065	4.05
2.20	.080	.100	9.00	0	.936	.06667	4.0
2.19	.083	.104	8.639	.036	.935	.06917	3.93
2.19	.085	.106	8.412	.059	.935	.07083	3.89
2.18	.088	.110	8.091	.091	.934	.07333	3.82
2.18	.090	.112	7.889	.111	.933	.075	3.78
2.17	.093	.116	7.602	.140	.932	.0775	3.72
2.17	.095	.119	7.421	.158	.932	.07917	3.68
2.16	.098	.122	7.163	.184	.931	.08167	3.63
2.16	.100	.125	7.0	.200	.930	.08333	3.59
2.15	.103	.129	6.767	.223	.929	.08583	3.54
	.105	.131	6.619	.238	.929	.0875	3.51
	.108	.135	6.407	.259	.928	.090	3.46
	.110	.138	6.273	.273	.925	.09167	3.43

$$\delta = 0,4$$

$\alpha$	$f_u$	$\sigma_u$	$\sigma_u'$	$f$	$q$	$C_u$
.113	.141	6.08	.292	.926	.09417	3.39
.115	.144	5.957	.304	.925	.09583	3.36
.118	.148	5.78	.322	.925	.09833	3.32
.120	.150	5.667	.333	.924	.100	3.29
.123	.154	5.504	.350	.923	.1025	3.25
.125	.156	5.400	.360	.922	.10417	3.23
.128	.160	5.25	.375	.922	.10667	3.19
.130	.163	5.154	.385	.921	.10833	3.17
.133	.166	5.015	.398	.920	.11083	3.13
.135	.169	4.926	.407	.919	.1125	3.11
.138	.173	4.797	.420	.919	.1150	3.08
.140	.175	4.714	.429	.918	.11667	3.06
.143	.179	4.594	.441	.917	.11917	3.03
.145	.181	4.517	.448	.917	.12083	3.00
.148	.185	4.405	.459	.916	.12333	2.98
.150	.188	4.333	.467	.915	.125	2.96
.153	.191	4.229	.477	.914	.1275	2.93
.155	.194	4.161	.484	.914	.12917	2.91
.158	.198	4.063	.494	.913	.13167	2.88
.160	.200	4.0	.500	.912	.1333	2.87
.163	.204	3.908	.509	.911	.13583	2.84
.165	.206	3.848	.515	.911	.1375	2.83
.168	.210	3.762	.524	.910	.140	2.80
.170	.213	3.706	.529	.909	.14167	2.79
.173	.216	3.624	.538	.908	.14417	2.76
.175	.219	3.571	.543	.908	.14583	2.75
.178	.222	3.494	.551	.907	.14833	2.73
.180	.225	3.444	.556	.906	.150	2.71
.183	.229	3.372	.563	.905	.1525	2.69
.185	.231	3.325	.568	.905	.15417	2.68
.188	.235	3.255	.574	.904	.15667	2.66
.190	.238	3.211	.579	.904	.15833	2.64
.193	.241	3.145	.585	.902	.16083	2.63
.193	.244	3.103	.590	.902	.1625	2.61
.198	.248	3.04	.596	.901	.165	2.59
.200	.25	3.0	.600	.900	.16667	2.58
.203	.254	2.941	.606	.899	.16917	2.56
.205	.256	2.902	.610	.898	.17083	2.55
.208	.260	2.846	.615	.898	.17333	2.53
.210	.262	2.81	.619	.897	.175	2.52
.213	.266	2.756	.624	.896	.1775	2.51
.215	.269	2.721	.628	.896	.17917	2.50
.218	.272	2.67	.633	.895	.18167	2.48
.220	.275	2.636	.636	.894	.18333	2.47
.223	.279	2.587	.641	.894	.18583	2.45
.225	.281	2.556	.644	.893	.1875	2.44
.228	.285	2.509	.649	.892	.190	2.42
.230	.287	2.478	.652	.891	.19167	2.41
.233	.291	2.433	.657	.890	.19417	2.4
.235	.294	2.404	.660	.890	.19583	2.41
.238	.297	2.361	.664	.889	.19833	2.31
.240	.300	2.333	.667	.888	.200	2.3
.243	.304	2.292	.671	.887	.2025	2.3
.245	.306	2.265	.673	.887	.20417	2.3
.248	.310	2.226	.677	.886	.20667	2.3
.250	.312	2.2	.680	.884	.21083	2.3
.253	.316	2.162	.684	.884	.21083	2.3

$\delta=0,4$

Cu	$\alpha$	$\xi_u$	$\beta_u$	$\beta_u'$	$\zeta$	$\eta$	Cu
3.39							
3.36							
	.255	.319	2.137	.686	.884	.2125	2.31
3.32	.258	.322	2.101	.690	.883	.215	2.30
3.29	.260	.325	2.077	.692	.882	.21667	2.29
3.25	.263	.329	2.042	.696	.881	.21917	2.28
3.23	.265	.331	2.019	.698	.881	.22083	2.27
3.19	.268	.335	1.985	.701	.880	.22333	2.26
3.17	.270	.337	1.963	.704	.879	.225	2.25
3.13	.273	.341	1.93	.707	.878	.2275	2.24
3.11	.275	.344	1.909	.709	.878	.22917	2.23
3.08	.278	.347	1.878	.712	.877	.23167	2.22
3.06	.280	.350	1.857	.714	.876	.2333	2.21
3.03	.283	.354	1.827	.717	.875	.23583	2.20
3.00	.285	.356	1.807	.719	.875	.2375	2.19
2.98	.228	.360	1.778	.722	.874	.240	2.18
2.96	.290	.363	1.759	.724	.873	.24167	2.18
2.93	.293	.366	1.73	.727	.872	.24417	2.17
2.91	.295	.369	1.712	.729	.871	.24583	2.16
2.88	.298	.372	1.685	.732	.871	.24833	2.15
2.87	.300	.375	1.667	.733	.870	.250	2.14
2.84	.303	.379	1.64	.736	.869	.2525	2.13
2.83	.305	.381	1.623	.738	.868	.25417	2.13
2.80	.308	.385	1.598	.740	.868	.25667	2.12
2.79	.310	.387	1.581	.742	.867	.25833	2.11
2.76	.313	.391	1.556	.744	.866	.26083	2.10
2.75	.315	.394	1.54	.746	.865	.2625	2.10
2.73	.318	.397	1.516	.748	.865	.265	2.09
2.71	.320	.400	1.500	.750	.864	.26667	2.08
2.69	.323	.404	1.477	.752	.863	.26917	2.07
2.68	.325	.406	1.462	.754	.863	.27083	2.07
2.66	.328	.410	1.439	.756	.862	.27333	2.06
2.64	.330	.412	1.424	.758	.861	.275	2.06
2.63	.333	.416	1.402	.760	.860	.2775	2.05
2.61	.335	.419	1.388	.761	.860	.27917	2.04
2.59	.338	.422	1.367	.763	.859	.28167	2.03
2.58	.340	.425	1.353	.765	.858	.28333	2.03
2.56	.345	.429	1.332	.767	.857	.28583	2.02
2.55	.345	.431	1.319	.768	.857	.2875	2.01
2.53	.348	.435	1.299	.770	.856	.290	2.01
2.52	.350	.437	1.286	.771	.855	.29167	2.00
2.51	.353	.441	1.266	.773	.854	.29417	2.00
2.50	.355	.444	1.254	.775	.854	.29583	1.99
2.48	.358	.447	1.235	.777	.853	.29833	1.98
2.47	.360	.450	1.222	.778	.852	.300	1.98
2.45	.363	.454	1.204	.780	.851	.3025	1.97
2.44	.365	.456	1.192	.781	.851	.30417	1.97
2.43	.368	.460	1.174	.783	.850	.30667	1.96
2.42	.370	.462	1.162	.784	.849	.30833	1.95
2.41	.373	.466	1.145	.786	.848	.31083	1.95
2.40	.375	.469	1.133	.787	.847	.3125	1.94
2.38	.378	.472	1.116	.788	.847	.315	1.94
2.37	.380	.475	1.105	.789	.846	.31667	1.93
2.36	.383	.479	1.089	.791	.845	.31917	1.93
2.35	.385	.481	1.078	.792	.844	.32083	1.92
2.34	.388	.485	1.062	.794	.844	.32333	1.91
2.33							
2.32							

$\delta=0,4$ 

$\alpha$	$f_u$	$\beta_u$	$\beta_u'$	$\zeta$	q	Cu
.393	.491	1.036	.796	.842	.3275	1.9
.395	.494	1.025	.797	.842	.32917	1.90
.398	.497	1.01	.799	.841	.33167	1.89
.400	.500	1.0	.800	.84	.3333	1.89
.403	.504	.985	.801	.839	.33583	1.88
.405	.506	.975	.802	.839	.3375	1.88
.408	.510	.961	.804	.838	.340	1.87
.410	.513	.951	.805	.837	.34167	1.87
.413	.516	.937	.806	.836	.34417	1.86
.415	.519	.928	.807	.836	.34583	1.86
.418	.523	.914	.809	.835	.34833	1.85
.420	.525	.905	.810	.834	.350	1.85
.423	.529	.891	.811	.833	.3525	1.85
.425	.531	.882	.812	.833	.35417	1.84
.428	.535	.869	.813	.832	.35667	1.84
.430	.538	.860	.814	.831	.35833	1.83
.433	.541	.848	.815	.830	.36083	1.83
.435	.544	.839	.816	.830	.3625	1.82
.438	.547	.826	.817	.829	.365	1.82
.440	.550	.818	.818	.828	.36667	1.81
.443	.554	.806	.819	.827	.36917	1.81
.445	.556	.798	.820	.827	.37083	1.81
.448	.560	.786	.821	.826	.37333	1.80
.450	.563	.778	.822	.825	.375	1.80
.453	.566	.766	.823	.824	.3775	1.79
.455	.569	.758	.824	.824	.37917	1.79
.458	.573	.747	.825	.823	.38167	1.78
.460	.575	.739	.826	.822	.38333	1.78
.463	.579	.728	.827	.821	.38583	1.78
.465	.581	.720	.828	.820	.3875	1.77
.468	.585	.709	.829	.820	.390	1.77
.470	.587	.702	.830	.819	.39167	1.77
.473	.591	.691	.831	.818	.39417	1.76
.478	.597	.674	.833	.817	.39833	1.75
.480	.600	.667	.833	.816	.400	1.75
.483	.604	.656	.834	.815	.4025	1.75
.485	.606	.649	.834	.815	.40417	1.74
.488	.610	.639	.836	.814	.40667	1.74
.490	.613	.633	.837	.813	.40833	1.74
.493	.616	.623	.838	.812	.41083	1.73
.495	.619	.616	.838	.812	.4125	1.73
.498	.623	.606	.839	.811	.415	1.72
.500	.625	.600	.840	.810	.41667	1.72
.530	.663	.509	.849	.801	.44167	1.68
.550	.688	.455	.855	.795	.45833	1.66

$\delta=0,6$

	$\alpha$	$\xi_u$	$\beta_u$	$\beta_u'$	$\xi$	$\eta$	$C_u$
	.055	.069	13.545	-.455	.929	.06875	3.96
	.058	.073	12.793	-.379	.928	.0725	3.86
Cu	.060	.075	12.333	-.333	.928	.075	3.79
	.063	.079	11.698	-.27	.927	.07875	3.7
1.9	.065	.081	11.308	-.231	.927	.08125	3.64
1.90							
1.89	.068	.085	10.765	-.176	.926	.085	3.56
1.89	.070	.088	10.429	-.143	.926	.0875	3.51
1.88	.073	.091	9.959	-.096	.925	.09125	3.44
1.88	.075	.094	9.667	-.067	.925	.09375	3.40
1.88	.078	.097	9.256	-.026	.924	.0975	3.33
1.87							
1.87	.080	.100	9.0	0	.924	.100	3.29
1.86	.083	.104	8.639	.036	.923	.10375	3.23
1.86	.085	.106	8.412	.059	.923	.10625	3.19
	.088	.110	8.091	.091	.922	.110	3.14
1.85	.090	.112	7.889	.111	.922	.1125	3.10
1.85							
1.85	.093	.116	7.602	.140	.921	.11625	3.06
1.84	.095	.119	7.421	.158	.921	.11875	3.02
1.84	.098	.122	7.163	.184	.920	.1225	2.98
	.100	.125	7.0	.200	.920	.125	2.95
1.83	.103	.129	6.767	.223	.919	.12875	2.91
1.83							
1.82	.105	.131	6.619	.238	.919	.13125	2.88
1.82	.108	.135	6.407	.259	.918	.135	2.84
1.81	.110	.138	6.273	.273	.918	.1375	2.81
	.113	.141	6.08	.292	.917	.14125	2.78
1.81	.115	.144	5.957	.304	.917	.14375	2.75
1.81							
1.80	.118	.148	5.78	.322	.916	.1475	2.72
1.80	.120	.150	5.667	.333	.916	.150	2.70
1.79	.123	.154	5.504	.350	.915	.15375	2.67
	.125	.156	5.40	.360	.915	.15625	2.64
1.79	.128	.160	5.25	.375	.914	.160	2.61
1.78							
1.78	.130	.163	5.154	.385	.914	.1625	2.59
1.78	.133	.166	5.015	.398	.913	.16625	2.57
1.77	.135	.169	4.926	.407	.913	.16875	2.55
	.138	.173	4.797	.420	.912	.1725	2.52
1.77	.140	.175	4.714	.425	.912	.175	2.50
1.77							
1.76	.143	.179	4.594	.441	.911	.17875	2.48
1.75	.145	.181	4.517	.448	.911	.18125	2.46
1.75	.148	.185	4.405	.459	.910	.1850	2.44
	.150	.188	4.333	.467	.910	.1875	2.42
1.75	.153	.191	4.229	.477	.909	.19125	2.40
1.74	.155	.194	4.161	.484	.909	.19375	2.38
1.74	.158	.198	4.063	.494	.908	.1975	2.36
1.74	.160	.200	4.0	.500	.908	.2	2.35
1.73	.163	.204	3.906	.509	.907	.20375	2.33
1.73	.165	.206	3.848	.515	.907	.20625	2.31
1.72							
1.72	.168	.210	3.762	.524	.906	.210	2.29
1.72	.170	.213	3.706	.529	.906	.2125	2.28
1.68	.173	.216	3.624	.538	.905	.21625	2.26
1.66	.175	.219	3.571	.543	.905	.21875	2.25
	.178	.222	3.494	.551	.905	.2225	2.23
	.180	.225	3.444	.556	.904	.225	2.22
	.183	.229	3.372	.563	.903	.22875	2.20
	.185	.231	3.324	.568	.903	.23125	2.19
	.188	.235	3.255	.574	.902	.235	2.17
	.190	.238	3.211	.579	.902	.2375	2.16
	.193	.241	3.145	.585	.901	.24125	2.14
	.195	.244	3.103	.590	.901	.24375	2.13
	.198	.248	3.04	.596	.9	.2475	2.12
	.200	.25	3	.600	.9	.2500	2.11
	.203	.254	2.941	.606	.899	.25375	2.09

$\alpha$	$\xi_u$	$\theta_u$	$\theta_u'$	$\zeta$	$q$	$C_u$
.205	.256	2.902	.610	.899	.25625	2.08
.208	.260	2.846	.615	.898	.260	2.07
.210	.262	2.81	.619	.898	.2625	2.06
.213	.266	2.756	.624	.897	.26625	2.05
.215	.269	2.721	.728	.897	.26875	2.04
.218	.272	2.67	.633	.896	.2725	2.02
.220	.275	2.636	.636	.896	.275	2.01
.223	.279	2.587	.641	.896	.27875	2.00
.225	.281	2.556	.644	.895	.28125	1.99
.228	.285	2.509	.649	.894	.285	1.98
.230	.287	2.477	.652	.894	.2875	1.97
.233	.291	2.433	.657	.893	.29125	1.96
.235	.294	2.404	.660	.893	.29375	1.95
.238	.297	2.361	.664	.892	.2975	1.94
.240	.300	2.333	.667	.892	.300	1.93
.243	.304	2.292	.671	.891	.30375	1.92
.245	.306	2.265	.673	.891	.30625	1.91
.248	.310	2.226	.677	.890	.310	1.90
.250	.312	2.2	.68	.89	.3125	1.90
.253	.316	2.162	.684	.889	.31625	1.89
.255	.319	2.137	.686	.889	.31875	1.88
.258	.322	2.101	.690	.888	.3225	1.87
.260	.325	2.077	.692	.888	.325	1.86
.263	.329	2.042	.696	.887	.32875	1.85
.265	.331	2.019	.698	.887	.33125	1.84
.268	.335	1.985	.701	.886	.335	1.84
.270	.337	1.963	.704	.886	.3375	1.83
.273	.341	1.93	.707	.885	.34125	1.82
.275	.344	1.909	.709	.885	.34375	1.81
.278	.347	1.878	.712	.884	.34375	1.80
.280	.350	1.857	.714	.884	.350	1.80
.283	.354	1.827	.717	.883	.35375	1.79
.285	.356	1.807	.719	.883	.35625	1.78
.288	.360	1.778	.722	.882	.360	1.77
.290	.363	1.759	.724	.882	.3625	1.77
.293	.366	1.73	.727	.881	.36625	1.76
.295	.369	1.712	.729	.881	.36875	1.75
.298	.372	1.685	.732	.880	.3725	1.75
.300	.375	1.667	.733	.88	.375	1.74
.303	.379	1.64	.736	.879	.37875	1.73
.305	.381	1.623	.738	.879	.38125	1.73
.308	.385	1.597	.740	.878	.375	1.72
.310	.387	1.581	.742	.878	.3875	1.71
.313	.391	1.556	.744	.877	.39125	1.71
.315	.394	1.54	.746	.877	.39375	1.70
.318	.397	1.516	.748	.876	.3975	1.69
.320	.400	1.5	.75	.876	.400	1.69
.323	.404	1.477	.752	.875	.40375	1.68
.325	.406	1.462	.754	.875	.40625	1.68
.328	.41	1.439	.756	.874	.410	1.67
.330	.412	1.424	.758	.874	.4125	1.67
.333	.416	1.402	.760	.873	.41625	1.66
.335	.419	1.388	.761	.873	.41875	1.65
.338	.422	1.367	.763	.872	.4225	1.65
.340	.425	1.353	.765	.872	.425	1.64
.343	.429	1.332	.767	.871	.42875	1.64
.345	.431	1.319	.768	.871	.43125	1.63
.348	.435	1.299	.770	.870	.435	1.63
.350	.437	1.286	.771	.87	.4375	1.62
.353	.441	1.266	.773	.869	.44125	1.61

Cu		$\delta = 0,6$						
	$\alpha$	$\xi_u$	$\theta_u$	$\theta_u'$	$G_u$	$q$	Cu	
2.08								
2.07	.355	.444	1.254	.775	.869	.44375	1.61	
2.06	.358	.447	1.235	.777	.868	.4475	1.60	
2.05	.360	.450	1.222	.778	.868	.450	1.60	
2.04	.363	.454	1.204	.78	.867	.45375	1.59	
2.02	.365	.456	1.192	.781	.867	.45625	1.59	
2.01	.368	.460	1.174	.783	.866	.460	1.58	
2.00	.370	.462	1.162	.784	.866	.4625	1.58	
1.99	.373	.466	1.145	.786	.865	.46625	1.57	
1.98	.375	.469	1.133	.787	.865	.46875	1.57	
1.97	.378	.472	1.116	.788	.864	.4725	1.57	
1.96	.380	.475	1.105	.789	.864	.475	1.56	
1.95	.383	.479	1.089	.791	.863	.47875	1.56	
1.94	.385	.481	1.078	.792	.863	.48125	1.55	
1.93	.388	.485	1.062	.794	.862	.485	1.55	
1.92	.390	.488	1.051	.795	.862	.4875	1.54	
1.91	.393	.491	1.036	.796	.861	.49125	1.54	
1.90	.395	.494	1.025	.797	.861	.49375	1.53	
1.90	.398	.497	1.01	.799	.860	.4975	1.53	
1.89	.400	.500	1.0	.800	.86	.500	1.53	
1.88	.403	.504	1.585	.801	.859	.50375	1.52	
1.87	.405	.506	.975	.802	.859	.50625	1.52	
1.86	.408	.510	.961	.804	.858	.510	1.51	
1.85	.410	.513	.951	.805	.858	.5125	1.51	
1.84	.413	.516	.937	.806	.857	.51625	1.50	
1.840	.415	.519	.928	.807	.857	.51875	1.50	
1.83	.418	.528	.914	.809	.856	.5225	1.50	
1.82	.420	.525	.905	.810	.856	.525	1.49	
1.81	.423	.529	.891	.811	.855	.52875	1.49	
1.80	.425	.531	.882	.812	.855	.53125	1.48	
1.80	.428	.535	.869	.813	.854	.535	1.48	
1.79	.430	.538	.860	.814	.954	.5375	1.48	
1.78	.433	.541	.848	.815	.853	.54125	1.47	
1.77	.435	.544	.839	.816	.853	.54375	1.47	
1.77	.438	.547	.826	.817	.852	.5475	1.46	
1.76	.440	.550	.818	.818	.852	.550	1.46	
1.75	.443	.554	.806	.819	.851	.55375	1.46	
1.75	.445	.556	.798	.820	.851	.55625	1.45	
1.74	.448	.560	.786	.821	.850	.5625	1.45	
1.73	.450	.563	.778	.822	.850	.5625	1.45	
1.73	.453	.566	.766	.823	.849	.56625	1.44	
1.72	.455	.569	.758	.824	.849	.56875	1.44	
1.71	.458	.573	.747	.825	.848	.5725	1.44	
1.71	.460	.575	.739	.825	.826	.848	1.43	
1.70	.463	.579	.728	.827	.847	.57875	1.43	
1.69	.465	.581	.720	.828	.847	.58125	1.43	
1.69	.468	.585	.709	.829	.846	.585	1.42	
1.68	.470	.587	.702	.830	.846	.5875	1.42	
1.68	.473	.591	.691	.831	.845	.59125	1.41	
1.67	.478	.597	.674	.833	.844	.5975	1.41	
1.67	.480	.600	.667	.833	.844	.600	1.41	
1.66	.483	.604	.656	.834	.843	.60375	1.40	
1.65	.485	.606	.649	.835	.843	.60625	1.40	
1.65	.488	.610	.639	.836	.842	.610	1.40	
1.64	.490	.613	.633	.837	.842	.6125	1.39	
1.64	.493	.616	.623	.838	.841	.61625	1.39	
1.63	.495	.619	.616	.838	.841	.61875	1.39	
1.63	.498	.623	.606	.839	.840	.6225	1.38	
1.62	.500	.625	.600	.840	.840	.625	1.38	
1.61	.530	.663	.509	.849	.834	.6625	1.35	
	.550	.688	.455	.855	.830	.6875	1.32	

$\delta = 0,8$

$\alpha$	$\xi_{11}$	$\theta_{11}$	$\theta_{11}'$	$\xi$	$q$	Cu
.055	.069	13.545	-.455	.915	.1375	2.82
.058	.073	12.793	-.379	.914	.145	2.75
.060	.075	12.333	-.333	.914	.150	2.70
.063	.075	11.698	-.270	.914	.1575	2.64
.065	.081	11.308	-.231	.913	.1625	2.60
.068	.085	10.765	-.176	.913	.170	2.54
.070	.088	10.429	-.143	.913	.175	2.50
.075	.091	9.9595	-.096	.913	.1825	2.45
.075	.094	9.667	-.067	.912	.1875	2.42
.078	.097	9.256	-.026	.912	.195	2.37
.080	.100	9.0	0	.912	.200	2.34
.083	.104	8.639	.036	.912	.2075	2.30
.085	.106	8.412	.056	.912	.2125	2.27
.088	.110	8.091	.091	.911	.22	2.23
.090	.112	7.889	.111	.911	.225	2.21
.093	.116	7.602	.140	.911	.2325	2.17
.095	.119	7.421	.158	.911	.2375	2.15
.098	.122	7.163	.184	.91	.245	2.12
.100	.125	7.0	.2	.91	.25	2.1
.103	.129	6.767	.223	.910	.2575	2.07
.105	.131	6.619	.238	.909	.2625	2.05
.108	.135	6.407	.259	.909	.270	2.02
.110	.138	6.273	.273	.909	.275	2.00
.113	.141	6.08	.292	.909	.2825	1.97
.115	.144	5.957	.304	.908	.2875	1.96
.118	.148	5.78	.322	.908	.295	1.93
.120	.150	5.667	.333	.908	.300	1.92
.123	.154	5.504	.350	.908	.3075	1.89
.125	.156	5.40	.360	.908	.3125	1.88
.128	.160	5.25	.375	.907	.320	1.86
.130	.163	5.154	.385	.907	.325	1.84
.133	.166	5.015	.398	.907	.3325	1.82
.135	.169	4.926	.407	.906	.3375	1.81
.138	.173	4.797	.420	.906	.345	1.79
.140	.175	4.714	.429	.906	.350	1.78
.143	.179	4.594	.441	.906	.3575	1.76
.145	.181	4.517	.448	.905	.3629	1.75
.148	.185	4.405	.459	.905	.370	1.73
.150	.188	4.333	.467	.905	.375	1.72
.157	.191	4.229	.477	.905	.3825	1.70
.155	.194	4.16	.484	.905	.3875	1.69
.158	.198	4.063	.494	.904	.395	1.67
.160	.200	4.0	.500	.904	.400	1.66
.163	.204	3.908	.509	.904	.4075	1.65
.165	.206	3.848	.515	.904	.4125	1.64
.168	.210	3.762	.524	.903	.420	1.62
.170	.213	3.706	.529	.903	.425	1.61
.173	.216	3.624	.538	.903	.4325	1.60
.175	.219	3.571	.543	.902	.4375	1.59
.178	.222	3.494	.551	.902	.445	1.58
.180	.225	3.444	.556	.902	.450	1.57
.183	.229	3.372	.563	.902	.4575	1.56
.185	.231	3.324	.568	.902	.4625	1.55
.188	.235	3.255	.574	.901	.470	1.54
.190	.238	3.211	.579	.901	.475	1.53
.193	.241	3.145	.585	.901	.4825	1.52
.195	.244	3.103	.590	.901	.4875	1.51
.198	.248	3.04	.596	.900	.495	1.50
.200	.250	3.0	.60	.900	.500	1.49
.203	.254	2.941	.606	.900	.5075	1.48



Cu	$\alpha$	$\rho_u$	$\rho_u$	$\rho_u'$	$\zeta$	q	Cu
2.82	.205	.256	2.902	.610	.899	.5125	1.47
2.75	.208	.260	2.846	.615	.899	.520	1.46
2.70	.210	.262	2.81	.619	.899	.525	1.46
2.64	.213	.266	2.756	.624	.899	.5325	1.45
2.60	.215	.269	2.721	.628	.898	.5375	1.44
2.54	.218	.272	2.67	.633	.898	.545	1.43
2.50	.22	.275	2.636	.636	.898	.550	1.42
2.45	.223	.279	2.587	.641	.898	.5575	1.41
2.42	.225	.281	2.556	.644	.898	.5625	1.41
2.37	.228	.285	2.509	.649	.897	.570	1.40
2.34	.230	.287	2.478	.652	.898	.575	1.39
2.30	.233	.291	2.433	.657	.897	.5825	1.38
2.27	.235	.294	2.404	.660	.896	.5875	1.38
2.23	.238	.297	2.361	.664	.896	.595	1.37
2.21	.240	.300	2.333	.667	.896	.600	1.36
2.17	.243	.304	2.292	.671	.896	.6075	1.36
2.15	.245	.306	2.265	.673	.895	.6125	1.35
2.12	.248	.310	2.226	.677	.895	.620	1.34
2.1	.250	.312	2.20	.680	.895	.625	1.34
2.07	.253	.316	2.162	.684	.895	.6325	1.33
2.05	.255	.319	2.137	.686	.895	.6375	1.32
2.02	.258	.322	2.101	.690	.894	.645	1.32
2.00	.260	.325	2.077	.692	.894	.650	1.31
1.97	.263	.329	2.042	.696	.894	.6575	1.30
1.96	.265	.331	2.019	.698	.894	.6625	1.30
1.93	.268	.335	1.985	.701	.893	.670	1.29
1.92	.270	.337	1.963	.704	.893	.675	1.29
1.89	.273	.341	1.93	.707	.893	.6825	1.28
1.88	.275	.344	1.909	.709	.892	.6875	1.28
1.86	.278	.347	1.878	.712	.892	.695	1.27
1.84	.280	.350	1.857	.714	.892	.700	1.27
1.82	.283	.354	1.827	.717	.892	.7075	1.26
1.81	.285	.356	1.807	.719	.891	.7125	1.26
1.79	.288	.360	1.778	.722	.891	.720	1.25
1.78	.290	.363	1.759	.724	.891	.725	1.24
1.76	.293	.366	1.73	.727	.891	.7325	1.24
1.75	.295	.369	1.712	.729	.891	.7375	1.23
1.73	.298	.372	1.685	.732	.890	.745	1.23
1.72	.300	.375	1.667	.733	.890	.750	1.22
1.70	.303	.379	1.640	.736	.890	.7575	1.22
1.69	.305	.381	1.623	.738	.889	.7625	1.21
1.67	.308	.385	1.597	.740	.889	.770	1.21
1.66	.310	.387	1.581	.742	.889	.775	1.20
1.65	.313	.391	1.556	.744	.889	.7825	1.20
1.64	.315	.394	1.54	.746	.888	.7875	1.20
1.62	.318	.397	1.516	.748	.888	.795	1.19
1.61	.320	.400	1.500	.750	.888	.800	1.19
1.60	.323	.404	1.477	.752	.888	.8075	1.18
1.59	.325	.406	1.462	.754	.888	.8125	1.18
1.58	.328	.410	1.439	.756	.887	.820	1.17
1.57	.330	.412	1.424	.758	.887	.825	1.17
1.56	.333	.416	1.402	.760	.887	.8325	1.16
1.55	.335	.419	1.388	.761	.887	.8375	1.16
1.54	.338	.422	1.367	.763	.886	.845	1.16
1.53	.340	.425	1.353	.765	.886	.850	1.15
1.52	.343	.429	1.332	.767	.886	.8575	1.15
1.51	.345	.431	1.319	.768	.885	.8625	1.14
1.50	.348	.435	1.299	.770	.885	.870	1.14
1.49	.350	.437	1.286	.771	.885	.875	1.14
1.48	.353	.441	1.266	.773	.885	.8825	1.13

$\delta = 0,8$

$\alpha$	$e_u$	$\rho_u$	$\rho_u'$	$q$	$q$	$C_u$
.355	.444	1.254	.775	.885	.8875	1.13
.358	.447	1.235	.777	.884	.895	1.12
.360	.450	1.222	.778	.884	.900	1.12
.363	.454	1.204	.780	.884	.9075	1.12
.363	.456	1.192	.781	.884	.9125	1.11
.368	.460	1.174	.783	.883	.920	1.11
.370	.462	1.162	.784	.883	.925	1.11
.373	.466	1.145	.786	.883	.9325	1.10
.375	.469	1.135	.787	.882	.9375	1.10
.378	.472	1.116	.788	.882	.945	1.10
.380	.475	1.105	.789	.882	.950	1.09
.383	.479	1.089	.791	.882	.9575	1.09
.385	.481	1.078	.792	.881	.9625	1.09
.388	.485	1.062	.794	.881	.970	1.08
.390	.488	1.051	.795	.881	.975	1.09
.393	.491	1.036	.796	.881	.9825	1.07
.395	.494	1.025	.797	.881	.9875	1.07
.398	.497	1.01	.799	.880	.995	1.07
.400	.500	1.0	.800	.88	1.0	1.07
.403	.504	.985	.801	.880	1.0075	1.06
.405	.506	.975	.802	.879	1.0125	1.06
.408	.510	.961	.804	.879	1.02	1.06
.410	.513	.951	.805	.879	1.025	1.05
.413	.516	.937	.806	.879	1.0325	1.05
.415	.519	.928	.807	.878	1.0375	1.05
.418	.523	.914	.809	.878	1.045	1.04
.420	.525	.905	.810	.878	1.05	1.04
.423	.529	.891	.811	.878	1.0575	1.04
.425	.531	.882	.812	.878	1.0625	1.04
.428	.535	.869	.813	.877	1.07	1.03
.430	.538	.860	.814	.877	1.075	1.03
.433	.541	.848	.815	.877	1.0825	1.03
.435	.544	.839	.816	.877	1.0875	1.02
.438	.547	.826	.817	.876	1.095	1.02
.440	.550	.818	.818	.876	1.1	1.02
.443	.554	.806	.819	.876	1.1075	1.02
.445	.556	.798	.820	.875	1.1125	1.01
.448	.560	.786	.821	.875	1.12	1.01
.450	.563	.778	.822	.875	1.125	1.01
.453	.566	.766	.823	.875	1.1325	1.00
.455	.569	.758	.824	.875	1.1375	1.00
.458	.573	.747	.825	.874	1.145	1.00
.460	.575	.739	.826	.874	1.15	1.00
.463	.579	.728	.827	.874	1.1575	.990
.465	.581	.720	.828	.874	1.1625	.99
.468	.585	.709	.829	.873	1.17	.99
.470	.587	.702	.830	.873	1.175	.99
.473	.591	.691	.831	.873	1.1825	.98
.478	.597	.674	.833	.872	1.195	.98
.480	.600	.667	.833	.872	1.200	.98
.483	.604	.656	.834	.872	1.2075	.97
.485	.606	.649	.835	.871	1.2125	.97
.488	.610	.639	.836	.871	1.220	.97
.490	.613	.633	.837	.871	1.225	.97
.495	.619	.616	.838	.871	1.2375	.96
.498	.623	.606	.840	.870	1.245	.96
.500	.625	.600	.840	.870	1.25	.96
.530	.663	.509	.849	.867	1.325	.93
.550	.688	.455	.855	.865	1.375	.92

LAMPIRAN I  
FAKTOR KONVERSI UNTUK SATUAN

0cm 46.78  
cm<sup>2</sup>

25

fil Bj37

Keterangan	satuan "US Custodary"	satuan SI		satuan MKS	
		satuan	faktor pengali	satuan	faktor pengali
<u>panjang</u>	inch	cm	2,54	cm	2,54
	ft	m	0,3048	m	0,3048
<u>luas:</u>	inch <sup>2</sup>	cm <sup>2</sup>	6,4516	cm <sup>2</sup>	6,4516
	ft <sup>2</sup>	m <sup>2</sup>	0,0929030	m <sup>2</sup>	0,0929030
<u>volume:</u>	inch <sup>3</sup>	cm <sup>3</sup>	16,387064	cm <sup>3</sup>	16,387064
	ft <sup>3</sup>	m <sup>3</sup>	0,0283168	m <sup>3</sup>	0,0283168
<u>berat</u>	lb	N(=New ton)	4,5	kgf	0,454
<u>density</u>	lb/ft <sup>3</sup>	kg/m <sup>3</sup>	16,0185	kg/m <sup>3</sup>	16,0185
	lb/in <sup>3</sup>	kg/m <sup>3</sup>	0,276799	kg/m <sup>3</sup>	0,276799
<u>beban</u>	lb/ft	N/m	14,6	kgf/m	1,48816
	lb/ft <sup>2</sup>	Pa(=Pascal)	47,9	kg/cm <sup>2</sup>	0,000488
<u>tegangan</u>	Psi	KPa (=kiloPascal)	6,9	kgf/cm <sup>2</sup>	0,07
<u>Gaya</u>	lbf	N	4,44822	kgf	0,454

Tambahan:

- (1) 1Pa = 1N/m<sup>2</sup>
- (2) 1kgf/m<sup>2</sup> = 9,80665 N/m<sup>2</sup>
- (3) 1 lb/in<sup>2</sup> = 689,76N/m<sup>2</sup>
- (4) 1 Mpa = 1000kPa = 145Psi
- (5) 1 kPa = 1000Pa

Catatan: maksudnya faktor pengali.

misal 1 Psi = 6,9 kPa = 0,07 kgf/cm<sup>2</sup>

balok  
akan  
adaan tsb?

.TA

DAFTAR HARGA SATUAN BAHAN BANGUNAN  
UNTUK BULAN : JUNI - JULI 1997/1998.

SUMBER DATA : PASARAN B E B A S  
D A E R A H : SEMARANG dan SEKITARNYA

Halaman : 1

No	JENIS BAHAN	SATUAN	H A R G A MINIMUM (Rp.)	MAKSIMUM (Rp.)	KETERANGAN
1	2	3	4	5	6
<b>I. BAHAN DASAR</b>					
1.	BATU KALI	Bulat utuh	m3	10.000	12.000
		Bulat belah	m3	16.000	18.000
		Pecah 5 / 7	m3	17.000	20.000
		Pecah 3 / 5	m3	18.000	21.000
		Pecah 2 / 3	m3	20.000	22.000
2.	KERIKIL	Timbun	m3	21.000	22.000
		Sawur/koral	m3	23.000	25.000
		Beton	m3	17.500	19.500
		Biasa	m3	10.000	11.000
		Trasc giling	m3	32.000	33.000
3.	BATU MERAH/BATA	Kwalltet II	bh	50	60
		Kwalltet I	bh	60	65
4.	PASIR	Urug	m3	8.000	9.500
		Pasang (bodri)	m3	12.000	17.000
		Beton (muntlan)	m3	21.000	22.000
		Tanah padas	m3	7.000	7.500
5.	KAPUR	Pasang	m3	28.000	30.000
		Sirih	m3	45.000	50.000
6.	PORTLAND CEMENT	Nusantara	zak	9.500	9.750
		Cibinong	zak	9.500	9.750
		Tiga roda	zak	9.500	9.750
		Gresik	zak	9.500	9.750
		White cement	zak	19.000	22.000
<b>II. BAHAN PENUTUP ATAP</b>					
1.	SIRAP	(100 LEMBAR)	pak	25.000	30.000
2.	GENTENG BETON				
		Genteng Beton Warna standart	bh	1.800	2.000
		Genteng Beton Warna Special	bh	1.900	2.250
		Genteng Beton Warna Khusus	bh	2.000	2.500
		Kerpus Warna Standart	bh	2.600	3.000
		Kerpus Warna Special	bh	2.700	3.250
		Kerpus Warna Khusus	bh	2.800	3.500
3.	GENTENG TANAH LIAT				
		Vlaam	bh	250	350
		Kodok	bh	300	500
		Nok kerpus	bh	400	700
4.	GENTENG KACA				
		Vlaam tebal 2 mm	bh	1.000	1.250
		Vlaam tebal 3 mm	bh	1.500	2.000
		Kodok tebal 2 mm	bh	2.250	2.500
		Kodok tebal 3 mm	bh	2.500	3.000
5.	ASBES GELOMBANG BESAR				
		Djâbes 6 1/2			
		. 200 cm X 110 cm X 5 mm	bh	20.000	22.500
		. 250 cm X 110 cm X 5 mm	bh	24.000	25.500
		. 225 cm X 110 cm X 5 mm	bh	21.000	23.000
		. 200 cm X 110 cm X 6 mm	bh	23.500	24.500
		. 225 cm X 110 cm X 6 mm	bh	26.000	27.500
		. 250 cm X 110 cm X 6 mm	bh	27.750	28.750

1	2	3	4	5	6
	Djabes 14 (Asbes Gelombang Kecil)				
	. 150 cm X 105 cm X 4 mm	bh	11.500	12.000	
	. 180 cm X 105 cm X 4 mm	bh	12.000	12.500	
	. 210 cm X 105 cm X 4 mm	bh	16.500	17.500	
	. 240 cm X 105 cm X 4 mm	bh	18.750	19.500	
	. 270 cm X 105 cm X 4 mm	bh	21.000	22.500	
	. 300 cm X 105 cm X 4 mm	bh	23.500	24.500	
6.	ASBES PLAT				
	Djabes Plat				
	. 100cm X 100 cm X 3 mm	lbr	3.500	4.500	
	. 30 cm X 200 cm X 3 mm	lbr	2.500	2.900	
	. 40 cm X 200 cm X 3 mm	lbr	3.000	4.000	
	. 50 cm X 200 cm X 3 mm	lbr	3.500	4.800	
	Jabes nok				
	. Kerpas Genteng	pcs	6.250	6.800	
	. Stel genteng	pcs	13.000	13.500	
	. Paten Besar 105 cm	pcs	7.500	8.500	
	Nokstel gelombang harflex				
	. Stel Besar 110 cm	pcs	15.500	17.000	
	. Patent Besar 110 cm	pcs	13.750	14.500	
	. Plat besar 110 cm	lbr	14.500	15.250	
7.	FIBRE GLASS (JABES)				
	180 X 92 cm	lbr	23.500	24.250	
	200 X 92 cm	lbr	30.500	31.250	
	250 X 92 cm	lbr	34.500	35.250	
	180 X 105 cm	lbr	21.200	21.950	
	210 X 105 cm	lbr	23.800	24.550	
	250 X 105 cm	lbr	32.500	33.250	
8.	SENG PLAT				
	BJLS 0,18	lbr	9.200	9.950	
	BJLS 0,20	lbr	10.500	11.250	
	BJLS 0,28	lbr	12.500	13.250	
	BJLS 0,30	lbr	13.800	14.550	
9.	SENG GELOMBANG				
	BJLS 0,18 panjang 180 cm	lbr	9.500	10.250	
	BJLS 0,20 panjang 180 cm	lbr	7.500	8.250	
	BJLS 0,30 panjang 180 cm	lbr	11.000	11.750	
	BJLS 0,40 panjang 180 cm	lbr	15.500	16.250	
<b>III. BAHAN KAYU</b>					
1.	JATI Papan	m3	2.500.000	4.500.000	semua ukuran
	Balok/pesagen	m3	1.900.000	4.250.000	semua ukuran
2.	KAMPER Papan	m3	1.200.000	1.250.000	semua ukuran
	Balok	m3	1.000.000	1.150.000	semua ukuran
3.	KRUWING Papan	m3	600.000	650.000	semua ukuran
	Balok	m3	525.000	575.000	semua ukuran
4.	MERANTI Papan	m3	500.000	550.000	semua ukuran
	Balok	m3	425.000	450.000	semua ukuran
5.	LANAN Papan	m3	195.000	200.000	
	Balok	m3	185.000	190.000	
6.	DOLKEN				
	Sedang 8 x 10 x 400 cm	btg	4.500	5.000	
	Keoll 6 x 7 x 400 cm	btg	3.000	4.000	
	Besar 10 x 12 x 400 cm	btg	4.000	4.500	
	Kayu cetakan	btg	55.000	60.000	
	Kayu bakar	m3	8.000	9.000	
7.	BENGGIRAI Papan	m3	700.000	725.000	
	Balok	m3	625.000	650.000	

1	2	3	4	5	6
<b>IV. BAHAN PENUTUP DINDING / LANTAI</b>					
<b>1. UBIN (TEGEL BIASA)</b>					
	PC polos	30 X 30 cm	m2	4.000	5.000
		20 X 20 cm	m2	3.500	4.000
	PC warna	30 X 30 cm	m2	7.500	8.000
		20 X 20 cm	m2	5.000	6.000
	Teraso	30 X 30 cm	m2	15.000	19.000
		20 X 20 cm	m2	11.000	14.000
<b>2. TEGEL PLINT</b>					
	PC warna	10 X 20 cm	bh	200	250
	Teraso		bh	600	700
<b>3. POLIS UBIN</b>					
	Lantai/badan		m2	1.250	1.500
	Plint		m'	550	650
	Trap		m'	800	900
<b>4. PASANG ALDAS DECORATIVE STONE</b>					
<b>5. UBIN PORSELIN</b>					
	Lokal	11 X 11	putih dos	10.000	12.000
		11 X 11	warna dos	15.000	16.000
	Lokal	15 X 15	putih dos	14.500	15.000
		15 X 15	warna dos	19.500	20.000
<b>6. MOZAIK PORSELIN</b>					
	10 X 20 cm	(diamond)	m2	10.000	14.200
	15 X 15 cm	(diamond)	m2	11.500	15.200
	20 X 20 cm	(diamond)	m2	12.000	15.200
	20 X 25 cm	(diamond)	m2	13.000	19.500
<b>7. Keramik</b>					
	30 X 30 cm		m2	12.000	15.000
<b>8. VINYL (Rol-rol an 1 x 2 m)</b>					
			m'	6.000	8.000
<b>9. KARPET</b>					
	Classic Ball		m2	39.000	41.000
	Nobel Long Life		m2	42.000	43.000
	Classic Hercules		m2	85.000	86.000
<b>V. BAHAN CETAK</b>					
<b>1. BUIS BETON Ø</b>					
	10 cm - 100 cm		bh	4.000	5.000
	20 cm - 100 cm		bh	6.500	7.000
	30 cm - 100 cm		bh	10.500	11.250
	50 cm - 100 cm		bh	20.000	21.000
	U 10 cm - 100 cm		bh	3.000	3.500
	U 15 cm - 100 cm		bh	4.000	4.500
	U 20 cm - 100 cm		bh	5.000	5.500
	U 30 cm - 100 cm		bh	6.500	7.000
	U 50 cm - 100 cm		bh	10.000	11.000
<b>2. LUBANG ANGIN (ROSTER) PC + PASIR</b>					
	10 X 20 cm		bh	200	950
	20 X 20 cm		bh	550	1.300
	25 X 25 cm		bh	800	1.550
	30 X 30 cm		bh	1.000	1.750
	15 X 25 cm		bh	500	1.250
	15 X 30 cm		bh	575	1.325
<b>VI. BAHAN BESI</b>					
<b>1. BESI BETON Ø</b>					
	4 mm - 12 m		btg	2.000	2.500
	6 mm - 12 m		btg	3.500	4.000
	8 mm - 12 m		btg	4.250	4.500
	10 mm - 12 m		btg	7.000	7.500
	12 mm - 12 m		btg	10.500	11.500
	16 mm - 12 m		btg	16.825	17.375
	19 mm - 12 m		btg	23.450	24.200
	25 mm - 12 m		btg	40.425	41.175

1	2	3	4	5	6
2.	<b>BESI PLAT</b>				
	3' X 6' tebal 0,6 mm	lbr	13.000	13.750	
	4' X 6' tebal 0,8 mm	lbr	30.000	35.000	
	4' X 8' tebal 1,4 mm	lbr	46.500	47.500	
3.	<b>BESI PROFIL</b>				
	Kanal UNP – 10 cm	btg	40.000	45.000	
	Kanal UNP – 12 cm	btg	65.000	70.000	
	Kanal UNP – 15 cm	btg	125.000	130.000	
	Kanal UNP – 20 cm	btg	180.000	190.000	
	Kanal IWF – 15 cm	kg	1.250	1.500	
	Kanal INP – 20 cm	kg	1.600	1.750	
4.	<b>JARING – JARING BAJA</b>				
	Diameter 4 – 15	kg	1.200	1.500	
	Diameter 6 – 15	kg	1.250	1.500	
5.	<b>BESI SIKU</b> L 40 X 40 X 4	btg	11.000	11.500	
	L 50 X 50 X 5	btg	17.000	17.500	
	L 60 X 60 X 6	btg	26.500	27.000	
6.	<b>KAWAT – ikat beton/bendrat</b>	kg	2.500	3.000	
	– Harmonika 12 X 45 mm	m2	2.000	4.000	
	– Harmonika 12 X 24 mm	m2	6.000	5.500	
	– Harmonika 14 X 30 mm	m2	6.500	7.000	
	– Harmonika 14 X 35 mm	m2	8.000	8.500	
	– Saringan pasir	m2	4.000	5.000	
	– Kawat loket	m2	4.000	5.000	
	– Kawat duri	rol	14.000	14.500	
<b>VII. BAHAN PIPA</b>					
1.	<b>PIPA PVC – Diameter</b>				
	– Diameter 1/2"	btg	4.000	6.000	
	– Diameter 3/4"	btg	6.000	7.500	
	– Diameter 1"	btg	5.500	10.800	
	– Diameter 2"	btg	16.000	27.200	
2.	<b>KNEE PVC – Diameter</b>				
	– Diameter 1/2"	bh	200	250	
	– Diameter 3/4"	bh	250	300	
	– Diameter 1"	bh	275	375	
3.	<b>PIPA GALVANIZED</b>		STR	MEDIUM	
	Diameter 1/2" – 6 m	btg	8.500	13.500	
	Diameter 3/4" – 6 m	btg	10.000	12.500	
	Diameter 1" – 6 m	btg	14.000	17.000	
	Diameter 1 1/2" – 6 m	btg	22.000	27.000	
	Diameter 2" – 6 m	btg	27.500	32.000	
	Diameter 2 1/2" – 6 m	btg	42.000	47.000	
	Diameter 3" – 6 m	btg	45.000	52.000	
	Diameter 4" – 6 m	btg	65.000	73.000	
4.	<b>PIPA MEDIUM</b>				
	Diameter 3" – 6 m	btg	80.000	85.500	
	Diameter 4" – 6 m	btg	125.000	130.000	
<b>VIII. BAHAN LANGIT – LANGIT</b>					
1.	<b>AKUSTIK – ukuran :</b>				
	30 X 30	lbr	2.000	4.000	
	30 X 60	lbr	4.500	5.000	
	40 X 40	lbr	6.000	7.000	
2.	<b>SOFT BOARD – ukuran :</b>				
	4'X 8'	lbr	13.000	14.500	
3.	<b>HARD BOARD – ukuran :</b>				
	4'X 8'	lbr	6.000	7.000	
4.	<b>PLY WOOD</b>				
	Teak wood				
	90 X 210 X 3 mm	lbr	13.000	14.000	

1	2	3	4	5	6
. 120 X 240	X 3 mm	lbr	17.000	18.000	
. 90 X 210	X 4 mm	lbr	14.500	15.000	
. 90 X 210	X 9 mm	lbr	21.000	24.000	
. 90 X 210	X 12 mm	lbr	28.500	30.000	
. 90 X 210	X 15 mm	lbr	33.000	37.500	
. 90 X 210	X 18 mm	lbr	39.000	42.000	
Tripleks					
. 120 X 240	X 3 mm	lbr	9.500	10.000	
. 120 X 240	X 4 mm	lbr	13.000	14.000	
. 120 X 240	X 6 mm	lbr	18.000	19.000	
Multipleks					
. 120 X 240	X 9 mm	lbr	29.000	30.000	
. 120 X 240	X 12 mm	lbr	34.000	35.000	
. 120 X 240	X 15 mm	lbr	43.000	44.000	
. 120 X 240	X 18 mm	lbr	47.500	48.500	

**IX. BAHAN FINISHING**

**1. KAYU**

Menle		kg	3.500	4.500
Dempul plamur		kg	3.000	5.000
Ambril/amples		lbr	350	400
Batu Apung		bh	250	500
Cat				
. Toyo		kg	6.500	7.000
. Yunlor 66 (nippon paint)		kg	4.750	5.000
. Primalin		ltr	1.750	2.000
. Deculux		kg	3.500	4.000
. Siratex		ons	1.900	2.500
. Spiritus		ltr	1.200	1.500
. Piltur jadi		ltr	4.800	5.200
. Herotex		ltr	2.000	2.250

**2. TEMBOK**

Kalkarium		kg	500	600
Kapur sirih		kg	200	300
Plamur	Toto	kg	2.000	3.000
	Decollth	5kg	8.000	9.000
Kimek	(Nippon paint)	5 kg	6.250	9.000
Matek	(Nippon paint)	5 kg	8.400	9.000
Toto		5 kg	8.800	17.000
Catylac		5 kg	11.750	12.000
Mowilex		5 kg	38.000	41.000

**3. BESI**

Menle	Patana	kg	3.500	4.500
Cat	Beebrand	kg	6.000	6.500
	Toyo paint	kg	4.000	5.000
Thinner A		ltr	2.400	2.700
Minyak cat		ltr	1.800	2.250
Thinner Super		ltr	2.500	3.000

**4. LAIN-LAIN**

Residu (teer/aspal)		drum	97.000	120.000
Fibre glass (tanki air)				
kapasitas 550 liter.		bh	162.000	180.000

**X. BAHAN KACA**

1. POLOS	Tebal :	2 mm	m2	8.500	9.000
		3 mm	m2	11.000	11.500
		5 mm	m2	13.500	14.000
		6 mm	m2	19.000	22.000
		8 mm	m2	31.000	35.000



1	2	3	4	5	6	
2. ES KABUR	Tebal :	2 mm	m2	7.500	8.000	
		3 mm	m2	12.500	13.000	
		5 mm	m2	18.000	18.500	
3. RAY BAND	Tebal :	3 mm	m2	15.000	16.500	
		5 mm	m2	19.500	20.500	
		8 mm	m2	47.500	48.500	
		10 mm	m2	53.500	55.000	
<b>XI. BAHAN INSTALASI LISTRIK</b>						
<b>1. KABEL LISTRIK</b>						
NYN : .	1 X 1 1/2 mm		m'	290	300	
				480	500	
				760	700	
NYY : .	2 X 1 1/2 mm		m'	1.100	1.200	
				1.700	2.000	
				2.300	2.500	
2. SKAKELAR	- Out baww .	Seri (broco)	bh	1.200	1.400	
				Engkel (broco)	800	1.000
		In baww .	Seri (broco)	bh	1.700	1.800
					Engkel (broco)	1.200
<b>3. FUSE BOX (SEKERING KASA)</b>						
1 group			bh	4.500	5.000	
2 group			bh	7.500	8.000	
3 group			bh	10.500	11.000	
<b>4. STEKER - Biasa (tunggal)</b>						
- Double			bh	350	400	
- Kombinasi kecil			bh	225	300	
- Kombinasi besar			bh	150	250	
- T			bh	850	900	
- T dengan arder			bh	500	600	
			bh	2.000	2.200	
<b>XII. ALAT - ALAT PENGUNCI &amp; PENGANTUNG</b>						
1. KUNCI TANAM	Union :	1 X slag	bh	7.500	9.000	
		2 X slag	bh	10.000	12.000	
	Yale :	1 X slag	bh	6.000	7.000	
		2 X slag	bh	17.500	18.000	
	Kuda :	1 X slag	bh	8.000	9.000	
		2 X slag	bh	9.750	11.000	
<b>2. ENGSEL DAN GERENDEL</b>						
Kupu-kupu biasa			bh	650	750	
Nylon kupu-kupu			bh	900	1.000	
Espagnoled - dalam negeri			bh	5.500	6.500	
Grendel Tanam luar negeri			bh	12.500	9.000	
<b>XIII. BAHAN SANITAIR (MERK INA)</b>						
1. KLOSET DUDUK	Type C - 4		bh	390.000	425.000 dg pembilas	
	Type C - 5		bh	490.000	530.000 dg pembilas	
	Type C - 13 T		bh	80.000	115.000 dg pembilas	
	Type C - 14 T		bh	80.000	115.000 dg pembilas	
	Type C - 27		bh	925.000	1.025.000 dg pembilas	
2. KLOSET JONGKOK	Type C - 1		bh	40.000	52.000	
	Type C - 2		bh	30.000	40.000	
	Type C - 3		bh	270.000	285.000 dg pembilas	
<b>3. WASTAFEL PEDESTAL 7,5 liter</b>						
Type L - 266 Wdk - 23 p			bh	570.000	625.000 dg kran air	
Type L - 266G - Wsk - 1 p			bh	370.000	425.000 dg kran air	
<b>4. WASTAFEL MEJA OVAL</b>						
Type L - 2594 WMK - 38M			bh	600.000	645.000 dg kran air	
Type L - 2394 WMK - 38M			bh	485.000	520.000	

1	2	3	4	5	6
	Type L -2296 WMK-38M	bh	565.000	600.000	
5.	WASTAFEL GANTUNG BULAT				
	Type L -286 WMK-38M	bh	470.000	485.000	body only
	Type L -284 WMK-38M	bh	470.000	485.000	body only
6.	WASTAFEL GANTUNG SUDUT				
	Type L -143	bh	44.000	77.000	body only
7.	WASTAFEL GANTUNG SUDUT KECIL				
	Type L -80	bh	40.000	46.000	body only
8.	WASTAFEL BAK CUCI				
	640x130x65 mm / Type H-401	bh	35.000	40.000	body only
9.	TEMPAT SABUN GANTUNG				
	210x110x 45 mm / Type H-411	bh	16.000	19.000	
	110x110x 45 mm / Type H-412	bh	11.000	13.500	
10.	TEMPAT SABUN TANAM				
	109x109x 95 mm / Type H- 25	bh	5.000	6.500	
	220x109x 90 mm / Type H- 27	bh	10.000	12.500	
11.	SEPTIC TANK (ETERNIT GRESIK)				
	5 Pemakai 500 liter	unit	115.000	120.000	
	10 Pemakai 1.000 liter	unit	147.000	150.000	
<b>XIV. ALAT PENGIKAT KAYU</b>					
1.	MUR BAUT (kuda-kuda)	kg	2.000	3.000	
2.	PAKU - ukuran 1" s/d 4"	kg	1.500	2.000	
3.	PAKU - payung	kg	2.000	2.500	
4.	PAKU - sekrup	gros	1.250	2.500	
5.	PAKU - beton	kg	1.500	2.000	
<b>XV. LAIN - LAIN BAHAN</b>					
1.	POMPA AIR TANGAN				
	Dragon buatan Korea	bh	45.000	50.000	
	Dragon buatan Jepang	bh	100.000	120.000	
	Dragon buatan Indonesia	bh	25.000	40.000	
2.	POMPA AIR LISTRIK				
	Sanyo 100 watt	bh	250.000	295.000	
	Fuji 250 watt	bh	130.000	140.000	
	Shimizu 100 watt	bh	170.000	190.000	
	90 watt	bh	150.000	175.000	
	D a b 125 watt	bh	110.000	120.000	aqua 125 A
	175 watt	bh	200.000	210.000	aqua 175 A
	200 watt	bh	200.000	210.000	miniJet 101A
	250 watt	bh	300.000	320.000	autosub 250
	375 watt	bh	541.000	545.000	aquaJet 375A
	500 watt	bh	835.000	845.000	aquaJet 501A
<b>XVI. PAVING BLOCK</b>					
1.	SQUARE				
	Abu-abu	bh	90	100	
	Merah/hitam	bh	135	145	
2.	HOLLAND				
	Abu-abu	bh	175	190	
	Merah/hitam	bh	245	260	
3.	UNIDECOR				
	Abu-abu	bh	230	250	
	Merah/hitam	bh	320	340	
4.	U N I				
	Abu-abu	bh	220	240	
	Merah/hitam	bh	305	325	
5.	TRIHEX				
	Abu-abu	bh	180	200	
	Merah/hitam	bh	225	275	
6.	OLYMPIA HEXA				
	Abu-abu	bh	325	355	
	Merah/hitam	bh	450	480	
7.	HEXAGONAL				
	Abu-abu	bh	300	330	
	Merah/hitam	bh	420	450	

1	2	3	4	5	6
8. CASTLE	Abu-abu	bh	850	1.150	
	Merah/hitam	bh	1.300	1.700	
9. TRAPEZ	Abu-abu	bh	480	520	
	Merah/hitam	bh	660	700	
10. TRAPEZ GRASS BLOCK					
	Abu-abu	bh	480	520	
	Merah/hitam	bh	660	700	
11. STANDARD GRASS BLOCK	Abu-abu	bh	2.895	3.085	
12. BATAKO		bh	600	710	
<b>XVII. LAIN - LAIN</b>					
1. KREI 25 MM		m2	22.500	27.500	
2. Sliding Pintu J3		btg	17.000	19.500	
Sliding Pintu J4		btg	20.000	24.500	
Sliding Pintu J5		btg	25.000	28.500	
3. Naco per Daun		bh	1.000	2.000	
4. Rolling door Besi		m2	27.500	30.000	
Rolling door Almunium		m2	55.000	60.000	
5. Awning Almunium		m2	14.000	16.000	
6. Kusen Almunium 4" Putih		m'	15.000	16.500	
Kusen Almunium 4" Coklat		m'	16.500	18.500	
Kusen Almunium 3" Putih		m'	18.500	14.500	



BIC-PINPU

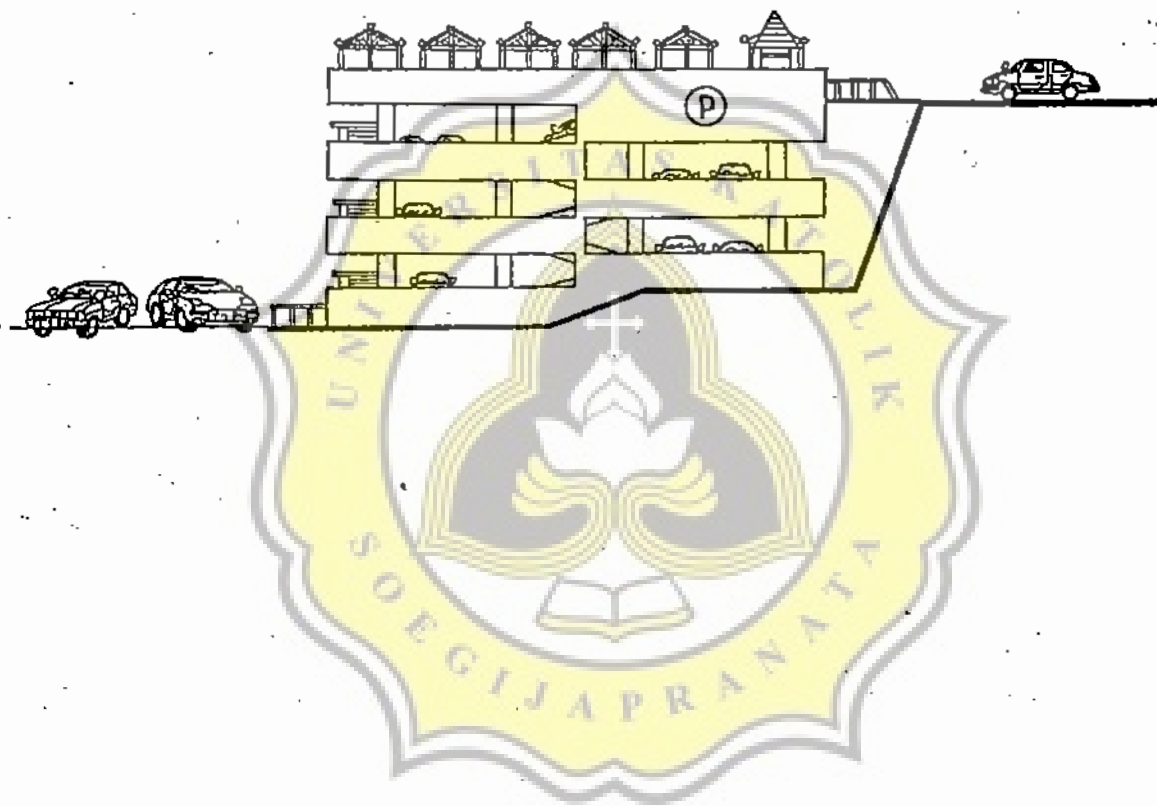
DAFTAR HARGA SATUAN UPAH TENAGA KERJA  
 UNTUK BULAN : JUNI - JULI 1997/1998.  
 SUMBER DATA : PASARAN B E B A S  
 D A E R A H : SEMARANG dan SEKITARNYA

Halaman : 9

No	U R A I A N	KODE	U P A H		KETERANGAN
			MINIMUM (Rp.)	MAKSIMUM (Rp.)	
01.	Pekerja	A( 1)/hr	6.000	6.500	
02.	Mandor	A( 2)/hr	6.000	6.500	
03.	Tukang listrik	A( 3)/hr	6.000	7.000	
04.	Tukang kayu	A( 4)/hr	7.000	8.000	
05.	Kep. tk. kayu	A( 5)/hr	8.000	9.000	
06.	Tukang batu	A( 6)/hr	7.000	7.500	
07.	Kep. tk. batu	A( 7)/hr	7.500	8.000	
08.	Tukang besi	A( 8)/hr	7.000	7.500	
09.	Kep. tk. besi	A( 9)/hr	7.500	8.000	
10.	Tukang cat	A(10)/hr	7.000	7.500	
11.	Kep. tk. cat	A(11)/hr	7.500	8.000	
12.	Tukang plitur	A(12)/hr	7.000	7.500	
13.	Tukang jalan	A(13)/hr	7.500	8.000	
14.	Tukang gali	A(14)/hr	7.000	7.500	
15.	Tukang masak aspal	A(15)/hr	6.500	7.000	
16.	Tk. leldeng	A(16)/hr	6.500	7.000	
17.	Masinis	A(17)/hr	7.000	7.500	
18.	Pemb. Masinis	A(18)/hr	6.500	7.000	
19.	Penjaga api	A(19)/hr	6.000	6.500	



# SURAT-SURAT



PERENCANAAN GEDUNG PARKIR  
UNIVERSITAS KATOLIK SOEGIJAPRANATA  
SEMARANG



**JURUSAN TEKNIK SIPIL**  
**FAKULTAS TEKNIK UNIVERSITAS KATOLIK SOEGIJAPRANATA**

Jl. Pawiyatan Luhur IV/1 Bendan Dhuwur Semarang-50234  
 Telp. (024) 316167 - 316142 - 441705 - 441762  
 Fax. (024) 415429 Po. Box. 8033/SM  
 Badan Hukum : Yayasan Sandjojo

Nomor : A.48.04/207/UKS.04.2/IV/1997

11 April 1997

Lamp : 1 (satu)lembar

H a l : MOHON TUGAS AKHIR

Kepada : Yth. Bapak. Prof.Ir. Soediro  
 Dosen Pembimbing Tugas Akhir  
 Bagi Mahasiswa Jurusan Teknik Sipil  
 Unika Soegijapranata  
 S e m a r a n g.

Kami beritahukan dengan hormat, bahwa pada Semester Genap 1996/1997 ada beberapa Mahasiswa Jurusan Teknik Sipil Fakultas Teknik Unika Soegijapranata Semarang yang berhak mendapatkan Tugas Akhir / Desain.

Sehubungan dengan hal tersebut di atas, maka kami mohon kesediaan Bapak berkenan memberikan Tugas Akhir/ Desain bagi mahasiswa terlampir.

Kami beritahukan pula bahwa, penyelesaian tugas dalam waktu 3 (tiga) bulan mulai tugas keluar (diberi tugas). Apabila tidak selesai dapat diperpanjang maksimal 3 (tiga) bulan, selebihnya tugas akhir dianggap gugur.

Demikian pemberitahuan kami, atas perhatian dan kerjasamanya Bapak, diucapkan terimakasih.

  
 Ketua Panitia,  
  
 FAKULTAS TEKNIK  
 JURUSAN TEKNIK SIPIL  
 IR. IGN. DARMOYO

Tembusan : Yth,

- Asisten Pembimbing Tugas Akhir
- Dekan Fakultas Teknik
- Ka. B A A K

*Yth. Ap. W. Budi Setiyadi' MT  
 Harap dibuahkan TA yg tol sama  
 dgn kaser proktekniknya  
 Trima kasih*

hardtugasaki18/rn

*Soediro  
 17/4/97*

Lampiran Surat Nomor :  
A.48.04/207/UKS.04.2/IV/97

1. NAMA MAHASISWA : B. TIPLUK JATI ARYANI  
NIM/NIRM : 92.12.962/92.6.111.03010.50029  
JUDUL LAPORAN KERJA PRAKTEK : PEMBANGUNAN PASARAYA SRI RATU EX  
BAZAR JALAN PEMUDA SEMARANG.
2. NAMA MAHASISWA : SETYOWATI KRISTIAJI  
NIM/NIRM : 92.12.1026/92.6.111.03010.50074  
JUDUL LAPORAN KERJA PAKTEK : PEMBANGUNAN GROUND TANK PADA PRO  
YEK HOTEL CENTRA WONOSOBO PROPIN  
SI JAWA TENGAH.

KETUA PANITIA,



IR. IGN. DARMOYO,



**JURUSAN TEKNIK SIPIL**  
**FAKULTAS TEKNIK UNIVERSITAS KATOLIK SOEGIJAPRANATA**

Jl. Pawiyatan Luhur IV/1 Bendan Dhuwur Semarang-50234  
Telp. (024) 316167 - 316142 - 441705 - 441762  
Fax. (024) 415429 Po. Box. 8033/SM  
Badan Hukum : Yayasan Sandjojo

Nomor : A.48.04/207/UKS.04.2/IV/1997

11 April 1997

Lamp : 1 (Satu) lembar

H a l : MOHON TUGAS AKHIR


Kepada : Yth. Bapak. Ir. Budi Setiyadi, MT  
Asisten Pembimbing Tugas Akhir  
Bagi Mahasiswa Jurusan Teknik Sipil  
Unika Soegijapranata  
S e m a r a n g.

Kami beritahukan dengan hormat, bahwa pada Semester Genap 1996/1997 ada beberapa Mahasiswa Jurusan Teknik Sipil Fakultas Teknik Unika Soegijapranata Semarang yang berhak mendapatkan Tugas Akhir / Desain.

Sehubungan dengan hal tersebut di atas, maka kami mohon kesediaan Bapak berkenan memberikan Tugas Akhir/ Desain bagi mahasiswa terlampir.

Kami beritahukan pula bahwa, penyelesaian tugas dalam waktu 3 (tiga) bulan mulai tugas keluar (diberi tugas). Apabila tidak selesai dapat diperpanjang maksimal 3 (tiga) bulan, selebihnya tugas akhir dianggap gugur.

Demikian pemberitahuan kami, atas perhatian dan kerjasamanya Bapak, diucapkan terimakasih.

  
Ketua Panitia,  
IR. IGN. DARMOYO

Tembusan : Yth,

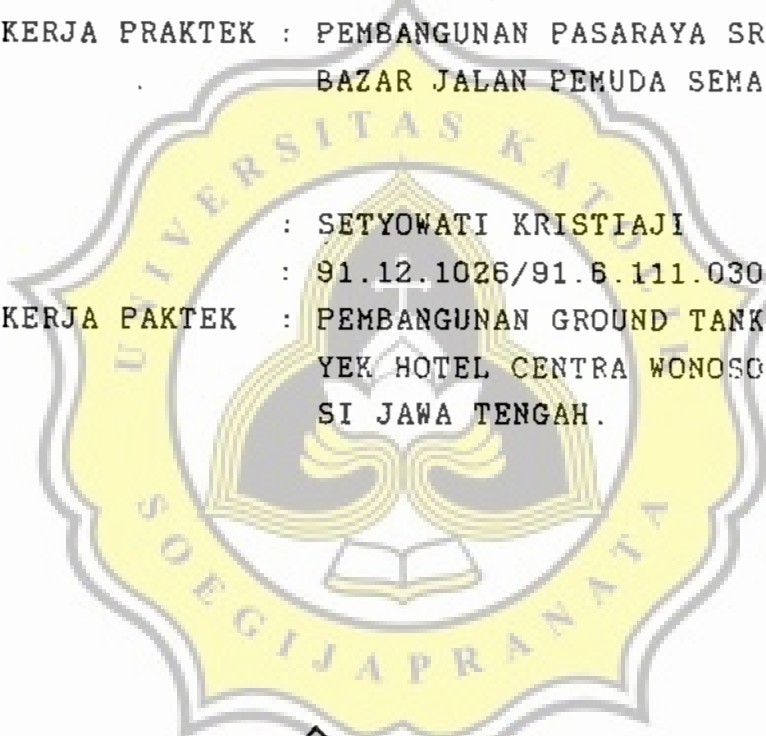
- Dekan Fakultas Teknik
- Ka. B A A K



Lampiran Surat Nomor :  
A.48.04/207/UKS.04.2/IV/97

1. NAMA MAHASISWA : B. TIPLUK JATI ARYANI  
NIM/NIRM : 91.12.962/91.6.111.03010.50029  
JUDUL LAPORAN KERJA PRAKTEK : PEMBANGUNAN PASARAYA SRI RATU EX  
BAZAR JALAN PEMUDA SEMARANG.

2. NAMA MAHASISWA : SETYOWATI KRISTIAJI  
NIM/NIRM : 91.12.1026/91.6.111.03010.50074  
JUDUL LAPORAN KERJA PAKTEK : PEMBANGUNAN GROUND TANK PADA PRO  
YEK HOTEL CENTRA WONOSOBO PROPIN  
SI JAWA TENGAH.



KETUA PANITIA,



IR. IGN. DARMOYO,